



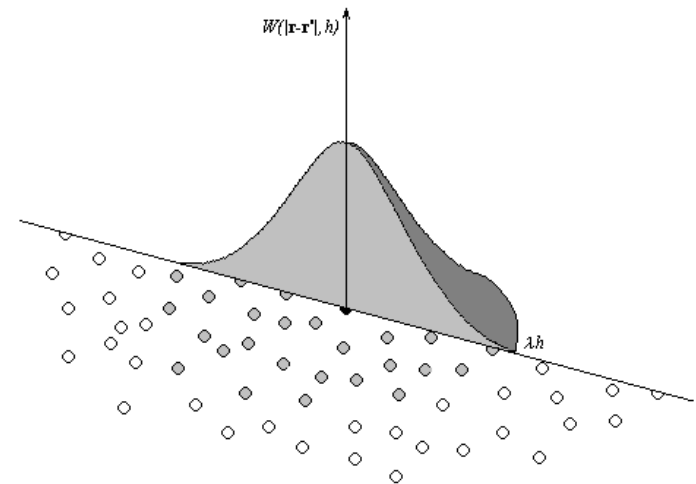
# Realistic Simulation through HPC: Application to Risk at Sea

A. Kamoulakos, P. Groenenboom  
ESI Group

B. Cartwright  
Pacific ESI



- Smoothed Particle Hydrodynamics (SPH)
- Meshless method for continuum mechanics
- Origins in modelling of cosmic physics
  - Gingold and Monaghan (1971)
- Proven in hypervelocity impact applications
- ESI version significantly enhanced for fluid-flow applications
  - Handles free-surface and other interfaces



# Special “interpolation” functions used called “smoothing functions”

Normalization

$$\int W(\mathbf{x} - \mathbf{x}', h) d\mathbf{x}' = 1$$

Compact support

$$W(\mathbf{x} - \mathbf{x}') = 0 \quad |\mathbf{x} - \mathbf{x}'| > \kappa h$$

Delta function property

$$\lim_{h \rightarrow 0} W(\mathbf{x} - \mathbf{x}', h) = \delta(\mathbf{x} - \mathbf{x}')$$

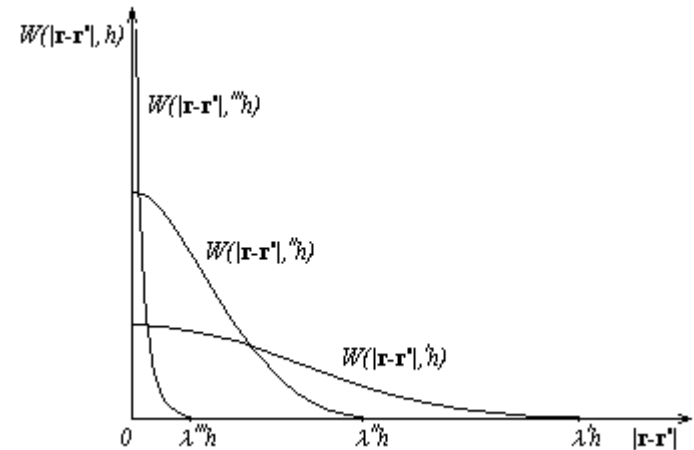
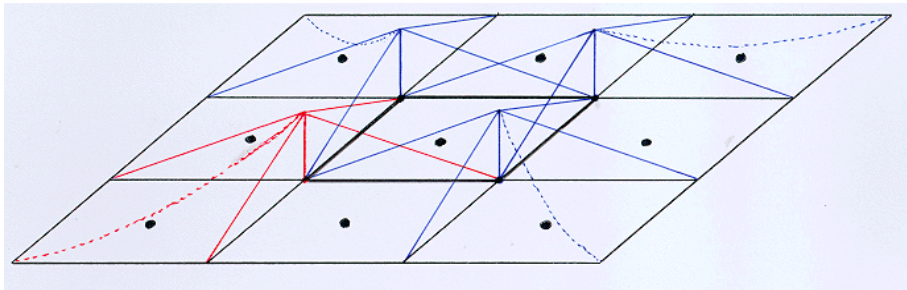
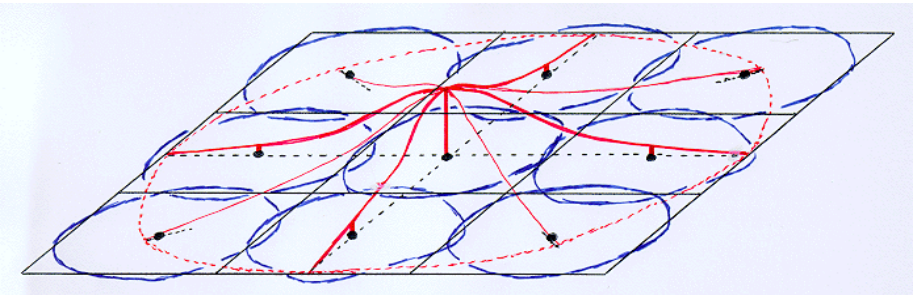


Illustration of smoothing functions



FE interpolation functions



SPH smoothing function

- Properties (eg. density) can be interpolated within a certain range.

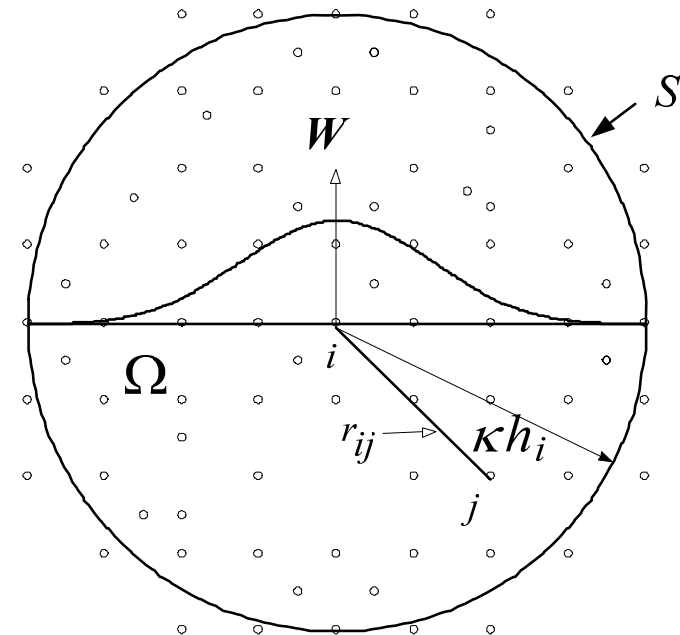
## ✓ Kernel approximation

$$f(x) = \int f(x')W(x-x',h)dx'$$

$$\nabla f(x) = \int f(x')\nabla W(x-x',h)dx'$$

**$h$  – Smoothing length**

**$W$  – Smoothing function**



- The interpolation points are identified with particles of a specified mass.

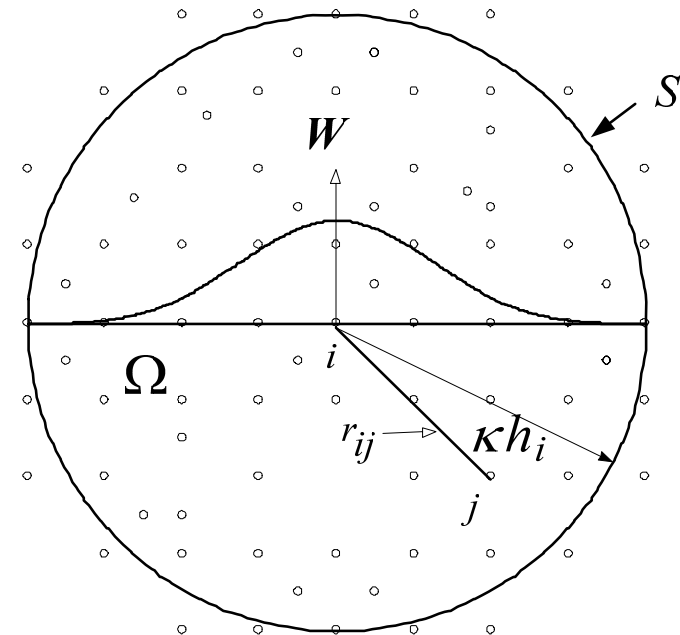
## ✓ Particle approximation

**$h$  – Smoothing length**

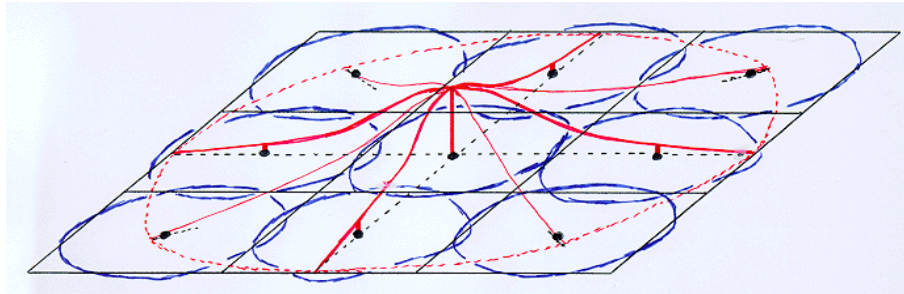
**$W$  – Smoothing function**

$$f_i = \sum_{j=1}^N \left( \frac{m_j}{\rho_j} \right) f_j W(x_i - x_j, h)$$

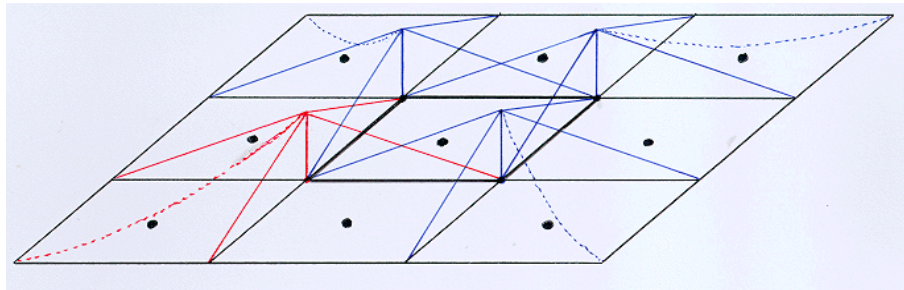
$$\nabla f_i = \sum_{j=1}^N \left( \frac{m_j}{\rho_j} \right) f_j \nabla_i W(x_i - x_j, h)$$



- The FE connectivity is replaced by a dynamic nearest neighbor search.



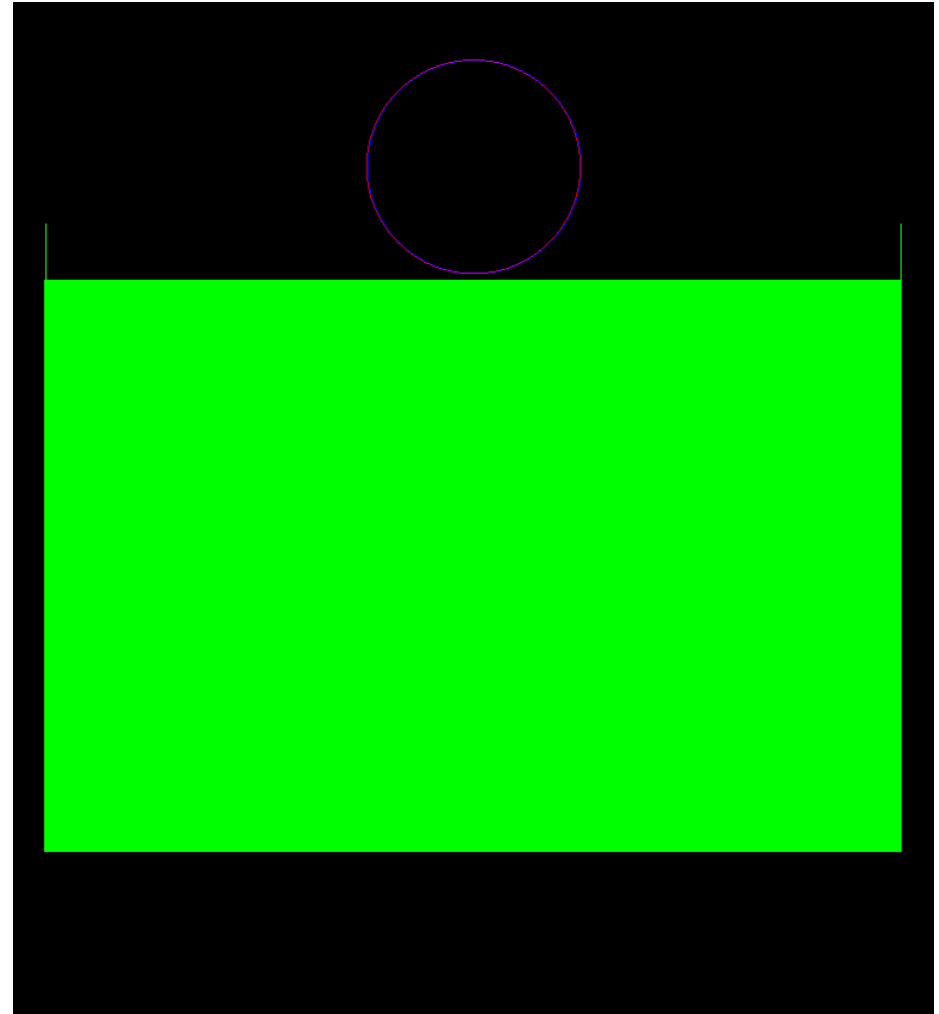
SPH neighborhood



FE connectivity

## Cylinder impacting fluid at constant speed

- The SPH method is fully integrated in the explicit finite element, crashworthiness code PAM-CRASH.
- A coupling between FE and SPH allows an interactive treatment of fluid-structure interaction.
- For regions with limited fluid displacements it is possible to use finite elements for the water.
  - See aircraft splashdown later on

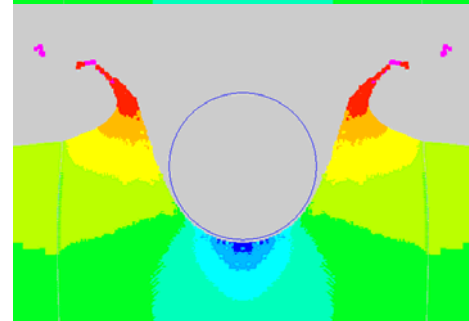
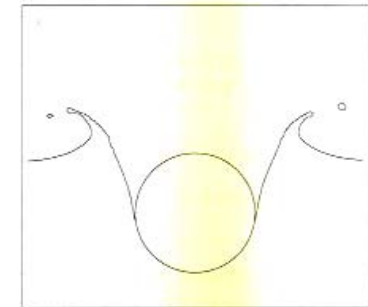
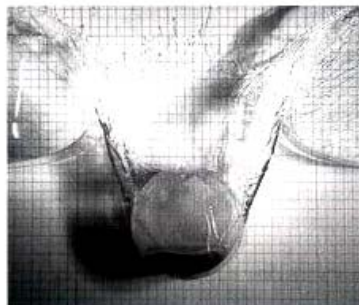
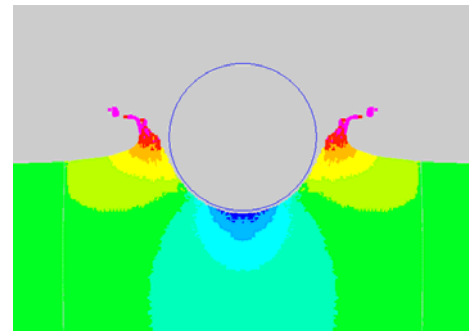
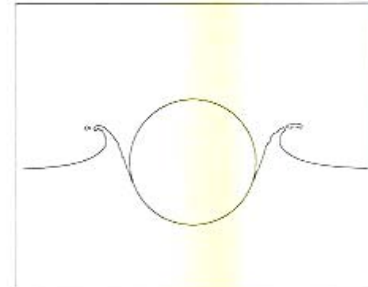
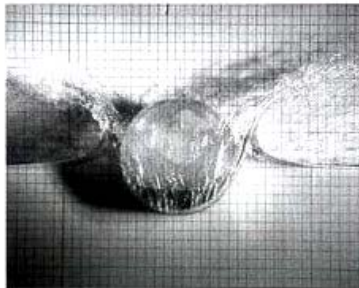
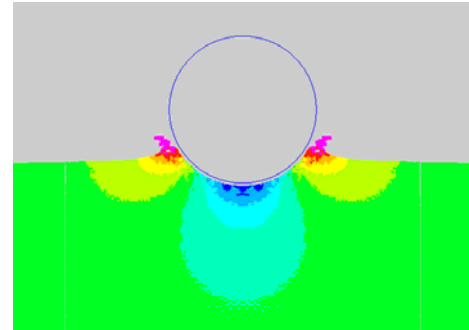
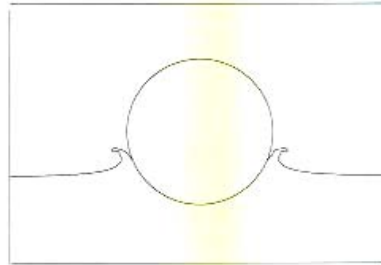
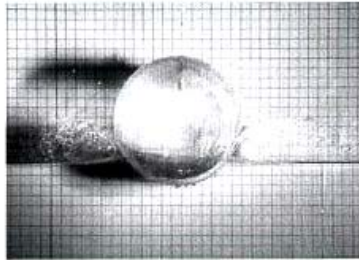


Contours represent velocity magnitude



# Cylinder impacting fluid at constant speed

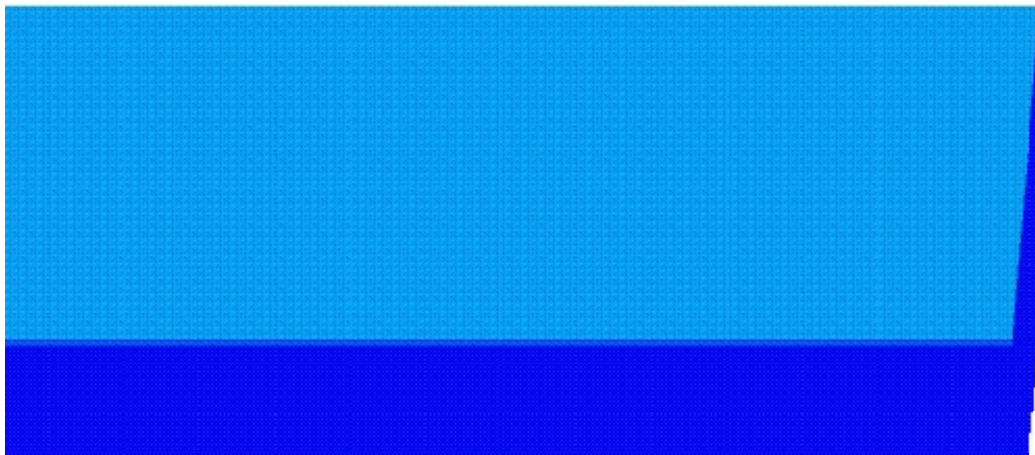
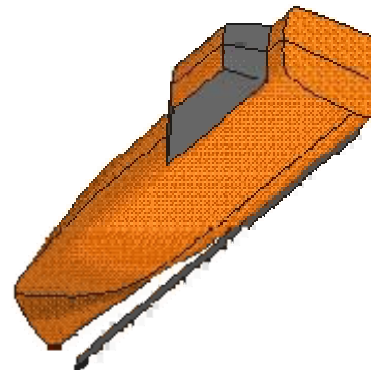
Free-surface deformation from Fekken (left) and for PAM-CRASH SPH/FE simulation with the contours of the velocity



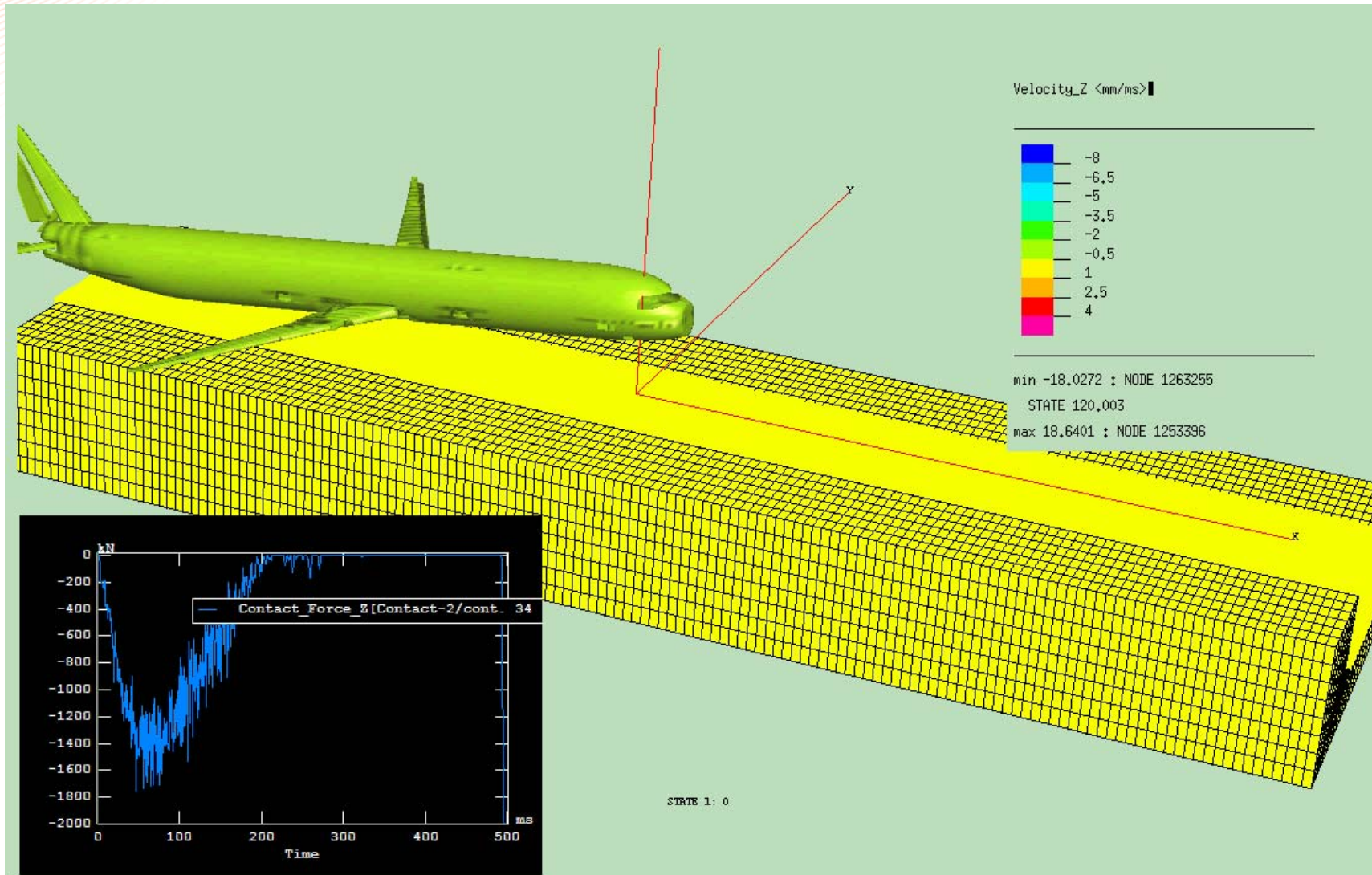


# Free fall of a lifeboat Limiting scenario

A commercial  
application

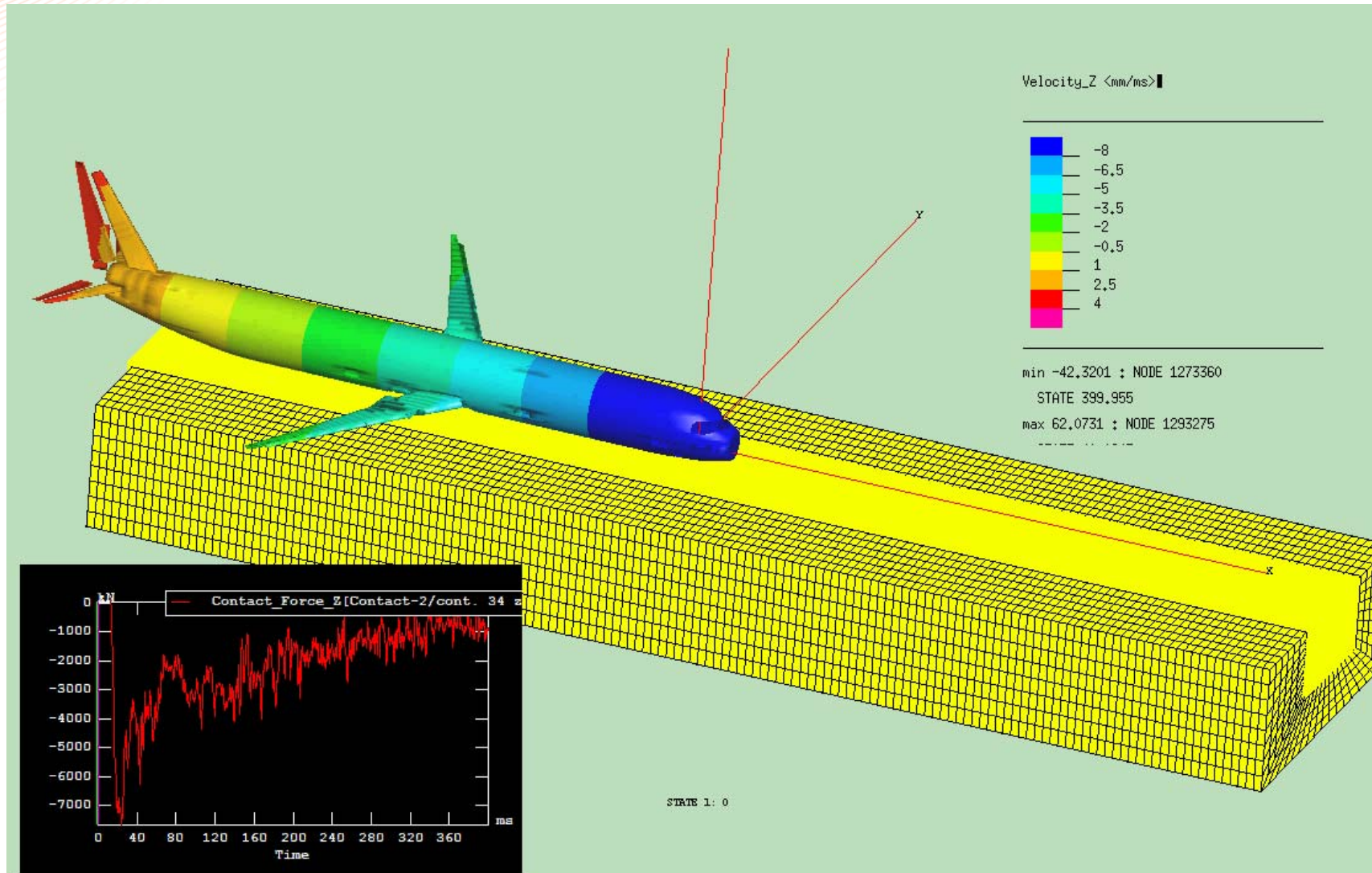


# (EC research project CRAHVI) Airbus 321 ditching (Courtesy of DLR)





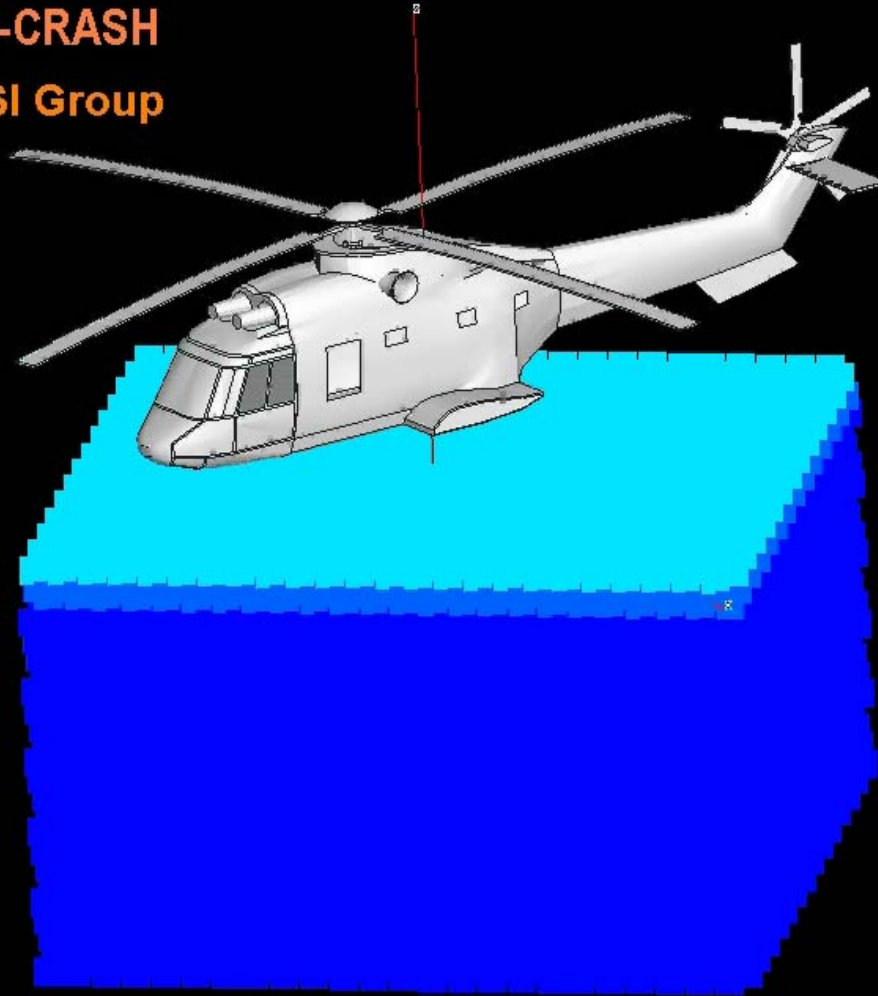
# (EC research project CRAHVI) Airbus 321 ditching (Courtesy of DLR)





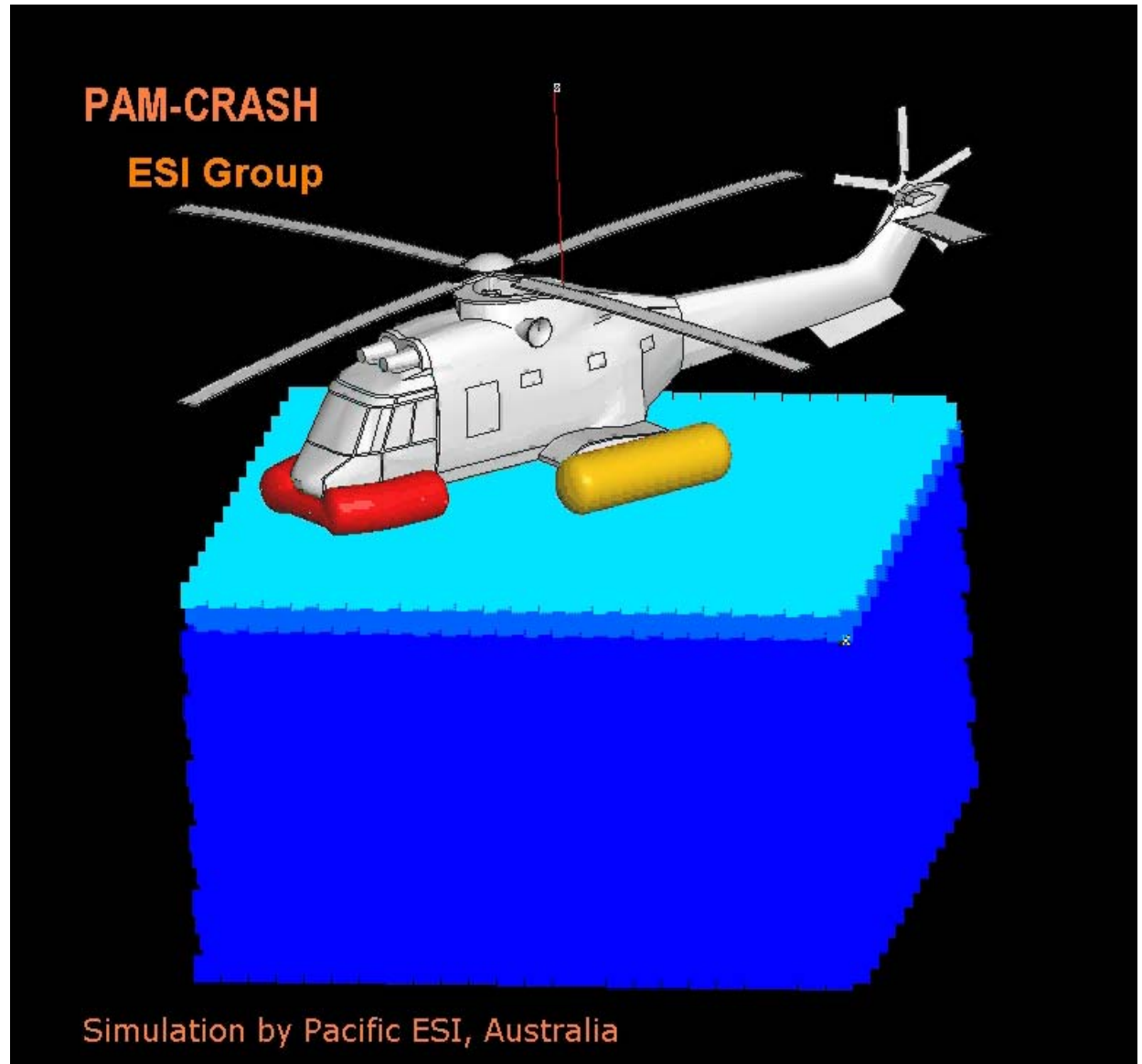
## Capsizing of Puma without airbags

**PAM-CRASH**  
**ESI Group**



Simulation by Pacific ESI, Australia

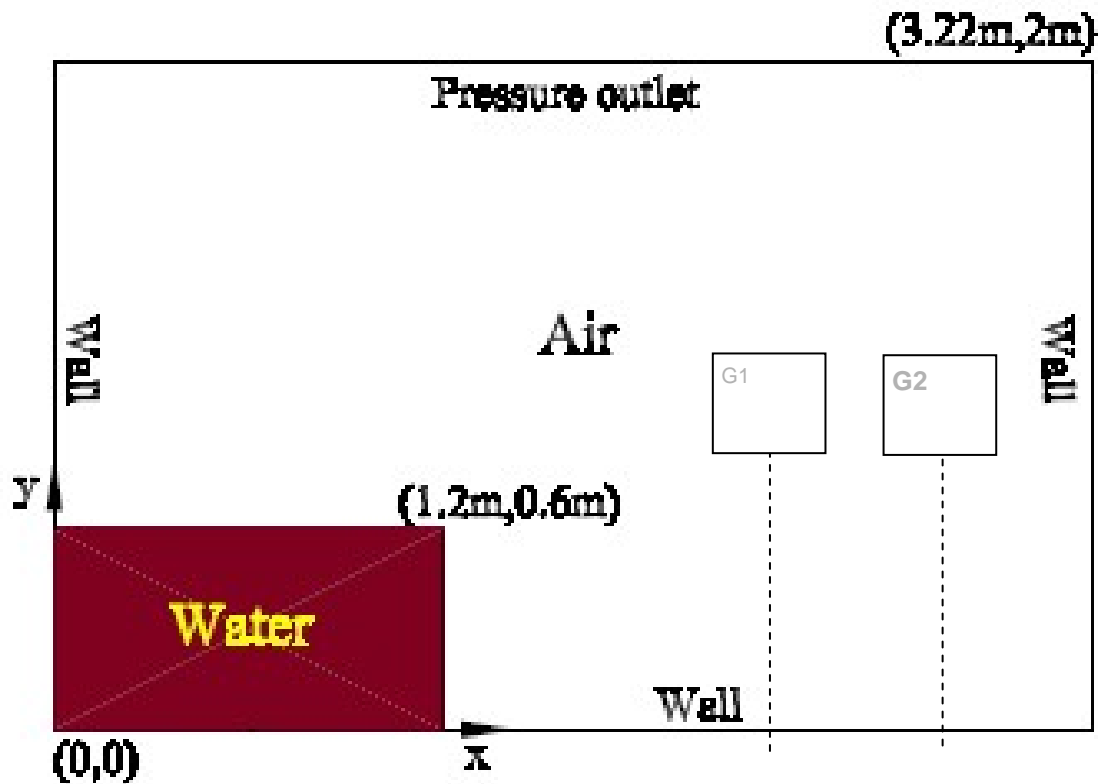
## Effect of airbags

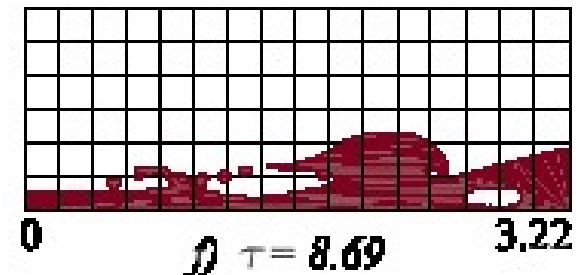
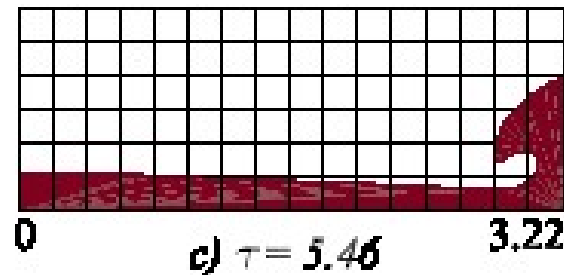
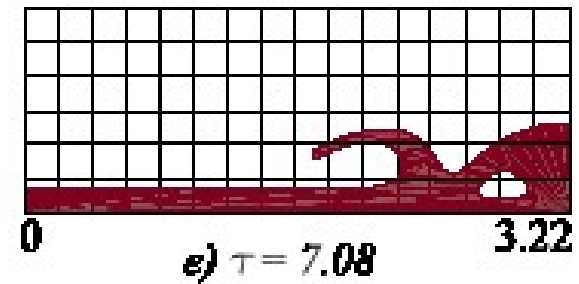
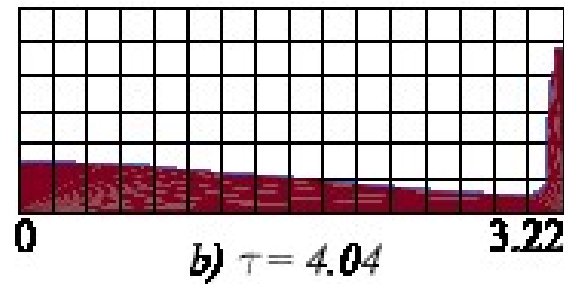
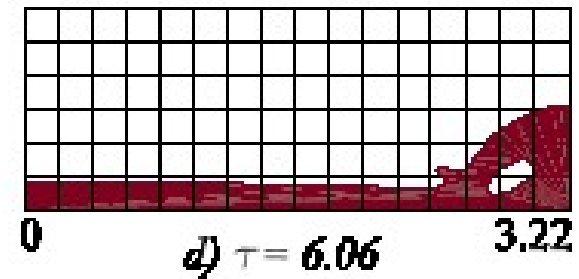
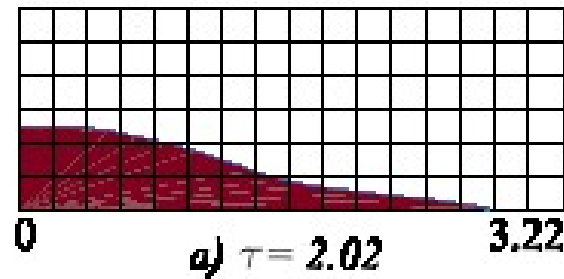


# Dam Break Benchmark

TEST: dam-break as described by Abdolmaleki, Thiagarajan and Morris-Thomas from the University of Western Australia at Crawley (2004) has been selected.

Important validation case and for particle size and SPH parameters.

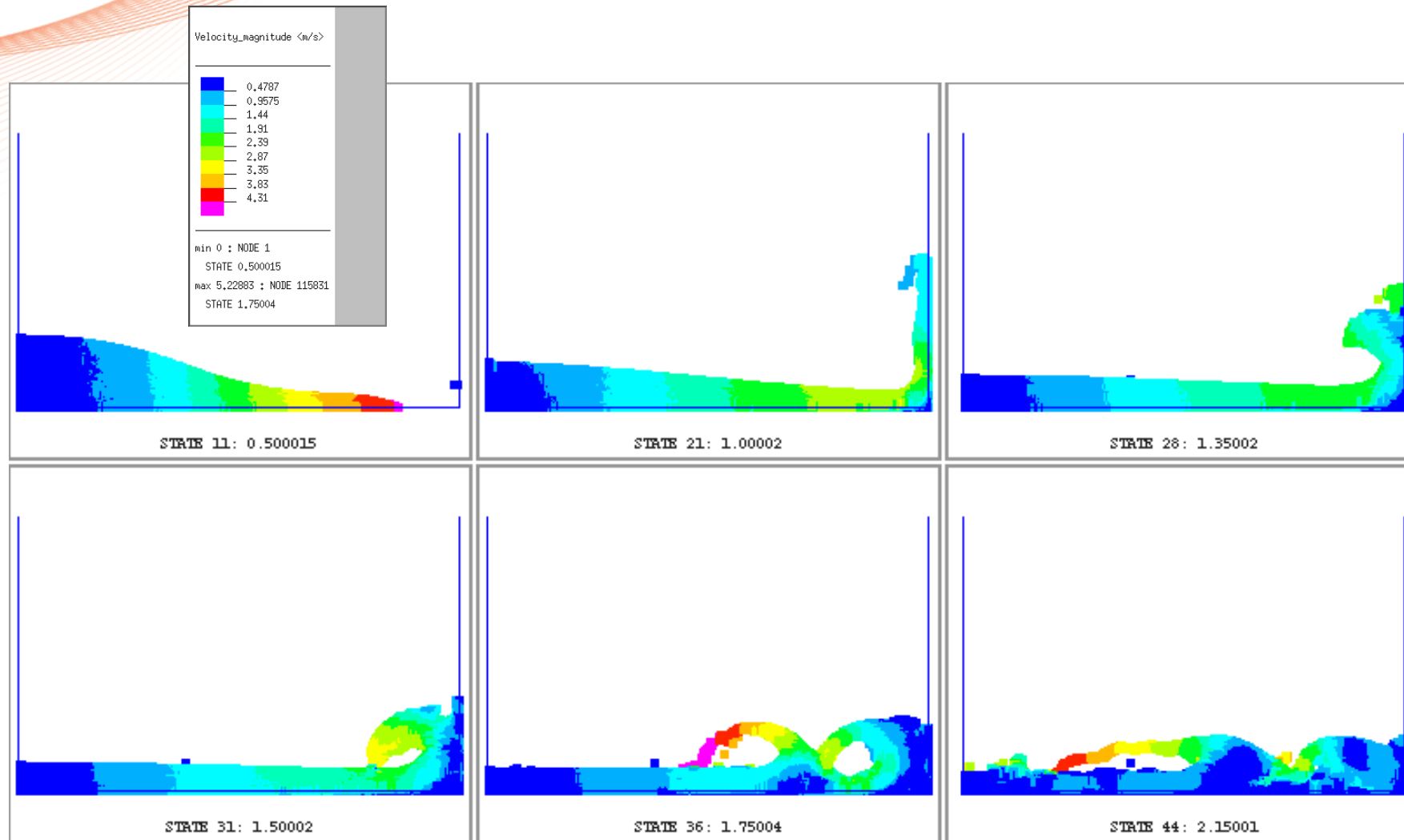




water contours as computed by FLUENT from Abdolmaleki et al.



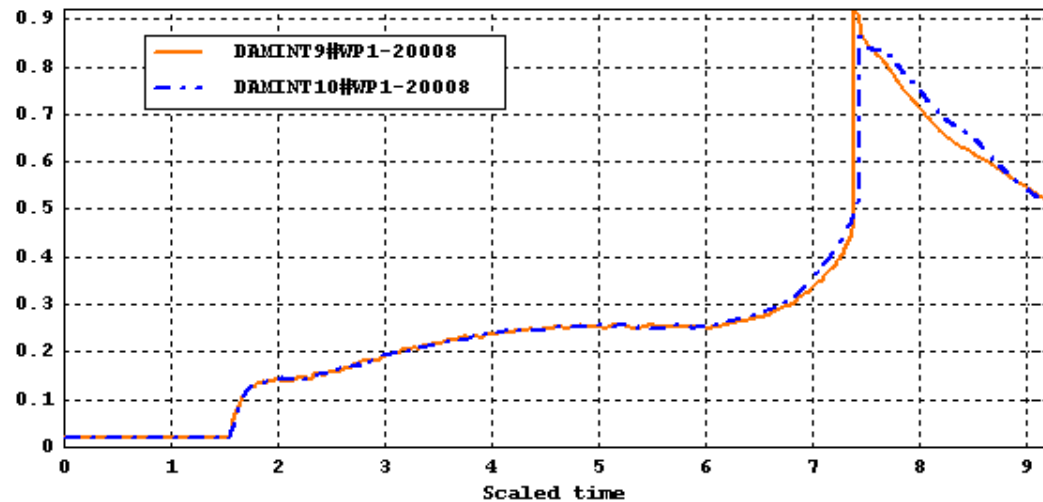
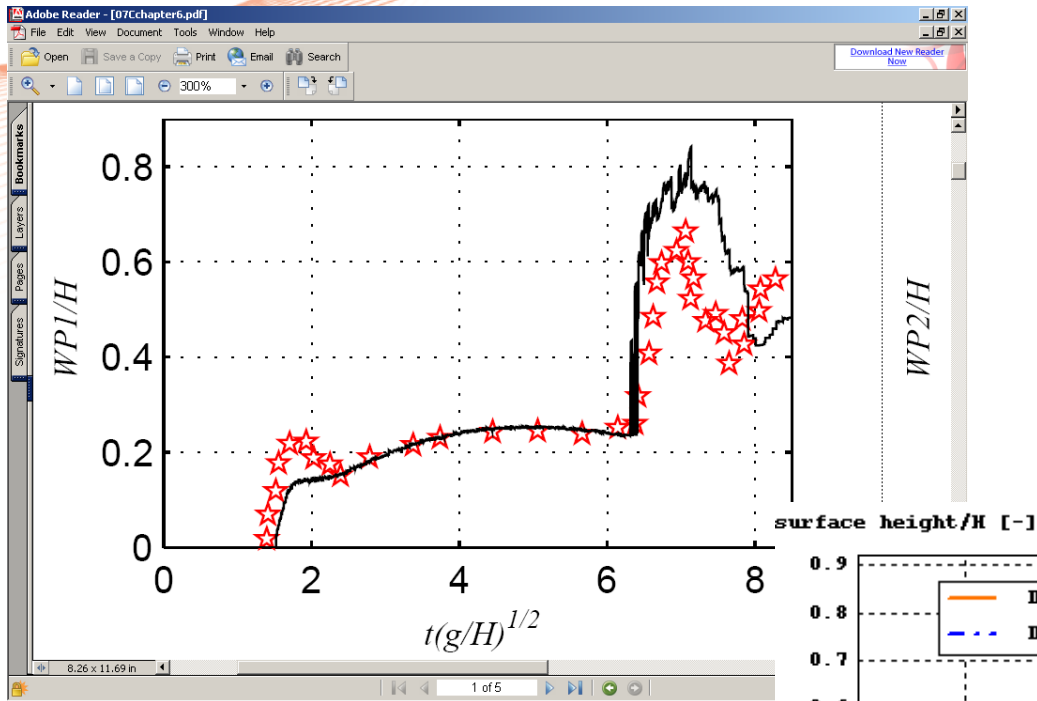
# DAM Break Simulation results



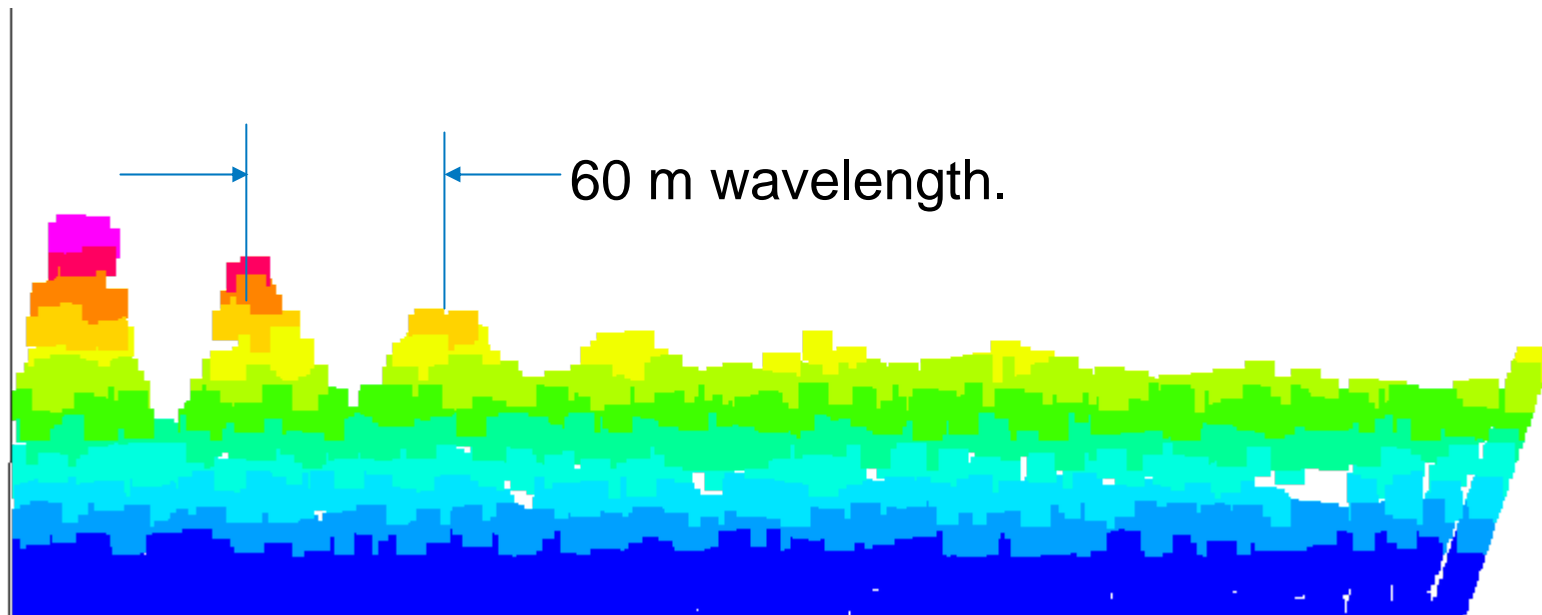
contour of the velocity at dimensionless time of 2.02, 4.04, 5.46, 6.06, 7.08 and 8.69

# Comparison of SPH with CFD

Free surface elevation (scaled)  
gauge 1 for two intermediate  
simulations.



Regular Wave Trials – not good

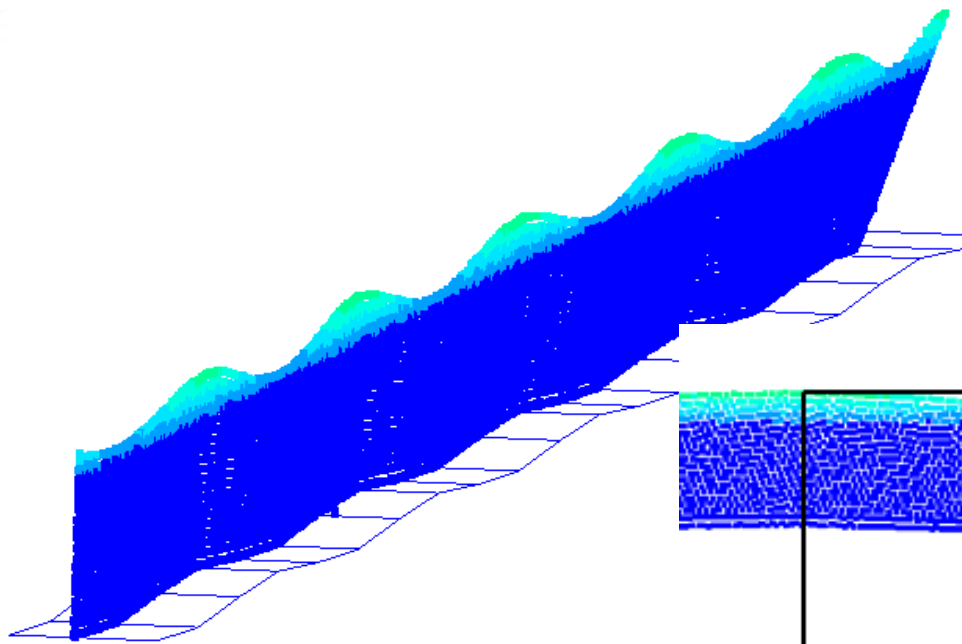


Colour represents vertical height  
(*Exaggerated vertical displacements*)

- For numerical solutions, modelling the wave to a depth where no motion occurs is costly, so we'd like to avoid it.
- If the modelling depth is less than half a wavelength, the solution for deep water waves will require special treatment of the sea-floor boundary.
- Rigid wall boundary conditions at this boundary are inconsistent with wave solutions for deep water.
- Moving the floor according to the motions of the wave theory has been found to reproduce the surface wave.

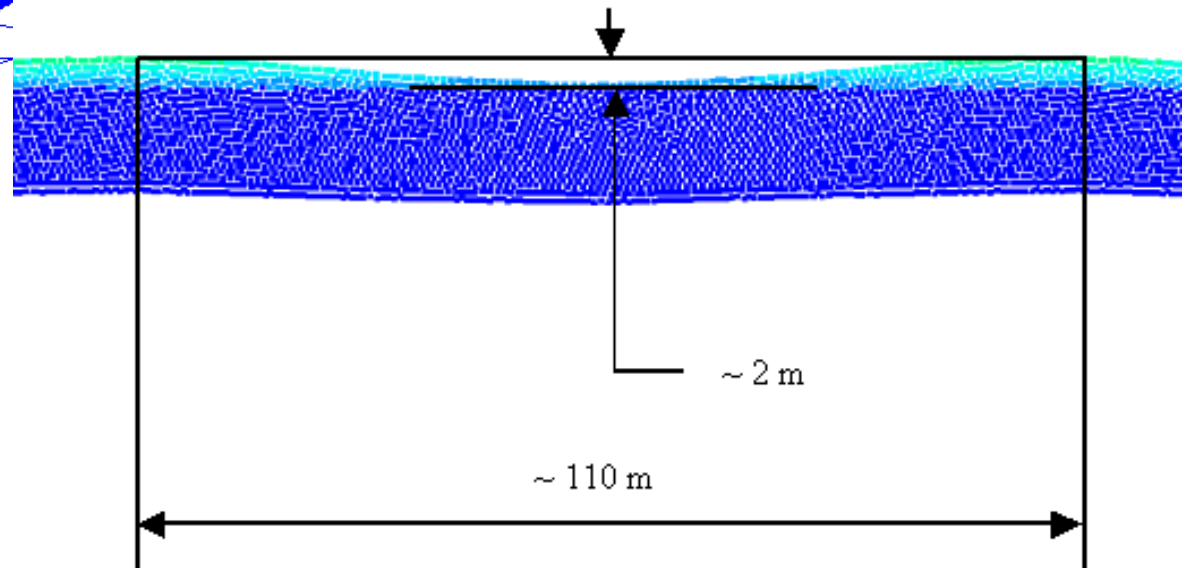


## Regular Wave Trials – Practical solution developed



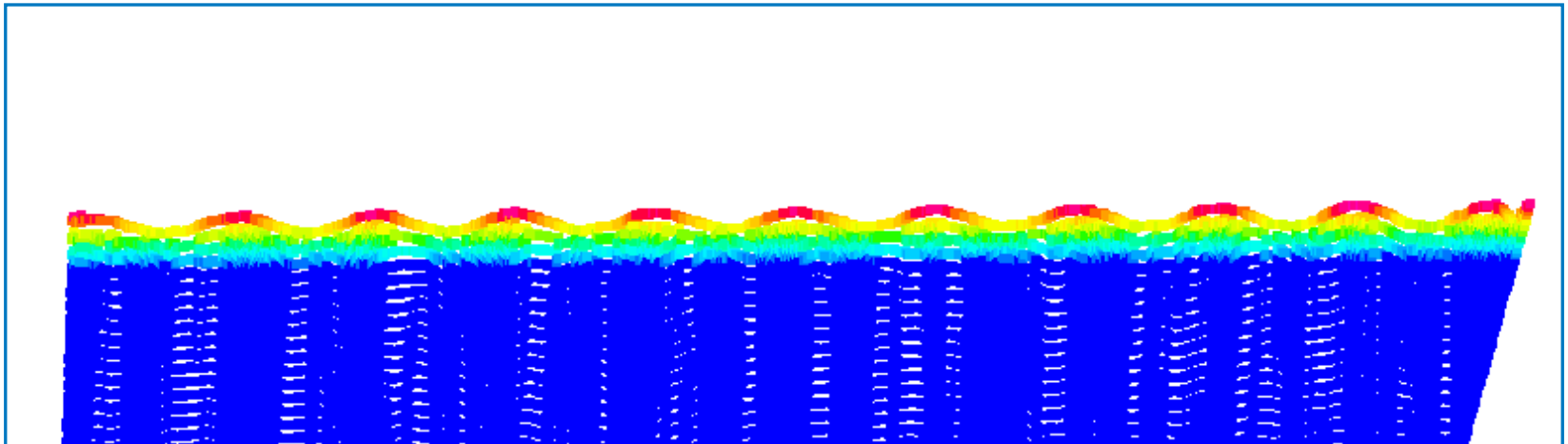
Wavelength = 110 metres

Depth = 15 metres

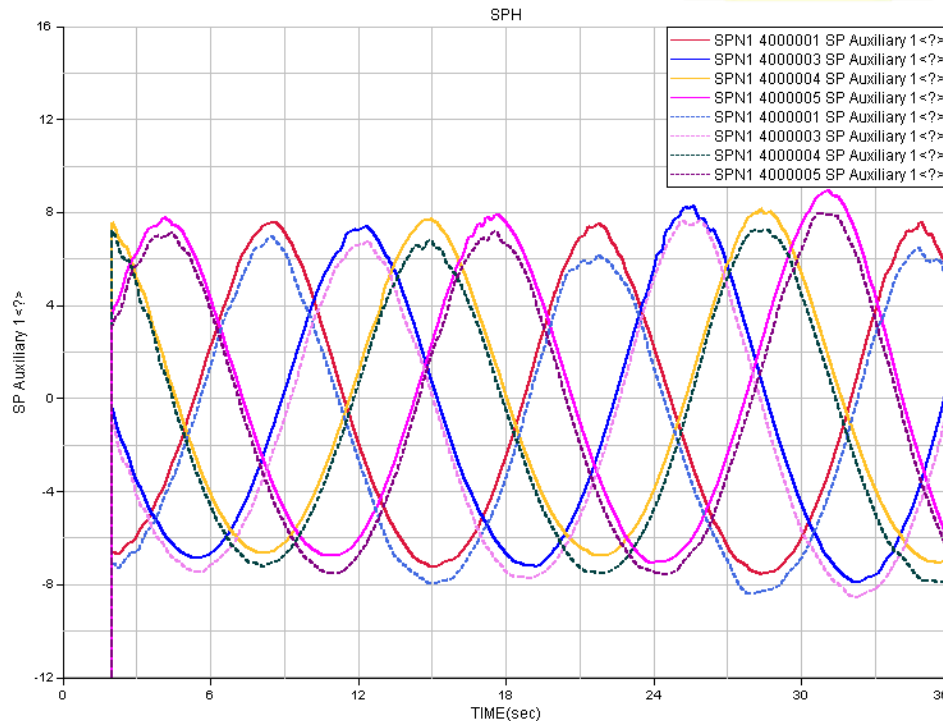
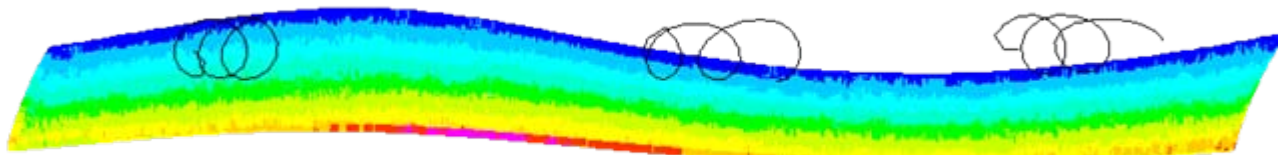


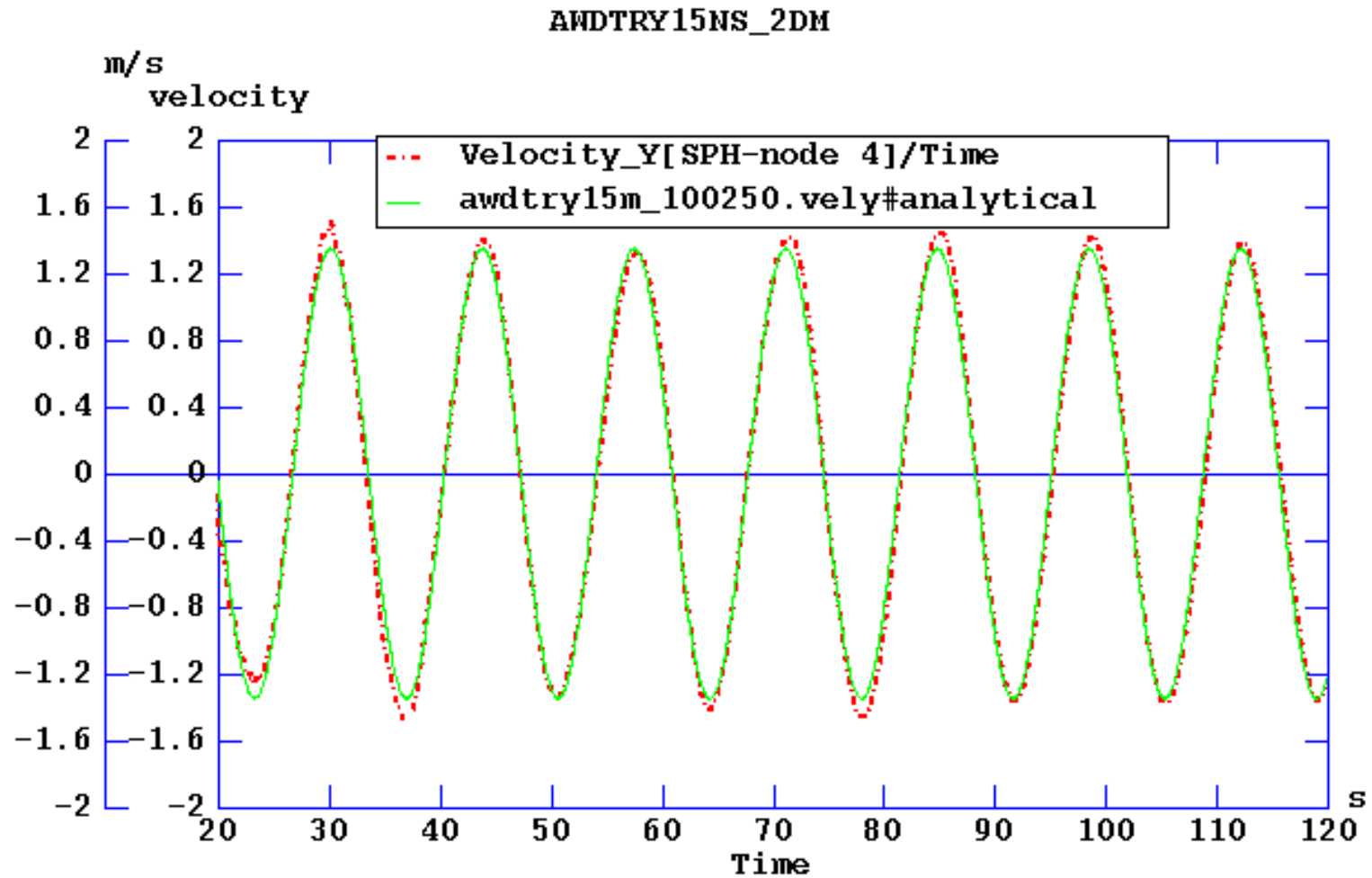
This concept permits a wave in a shallow tank to behave like a deep water wave. This allows a more CPU-efficient solution than the simple solution of modelling the complete depth.

Below is an example of 1km of a 1m amplitude wave of 100m wavelength in 15 metres of water. (*The view is oblique, to reveal the 1m amplitude, colour representing height.*)



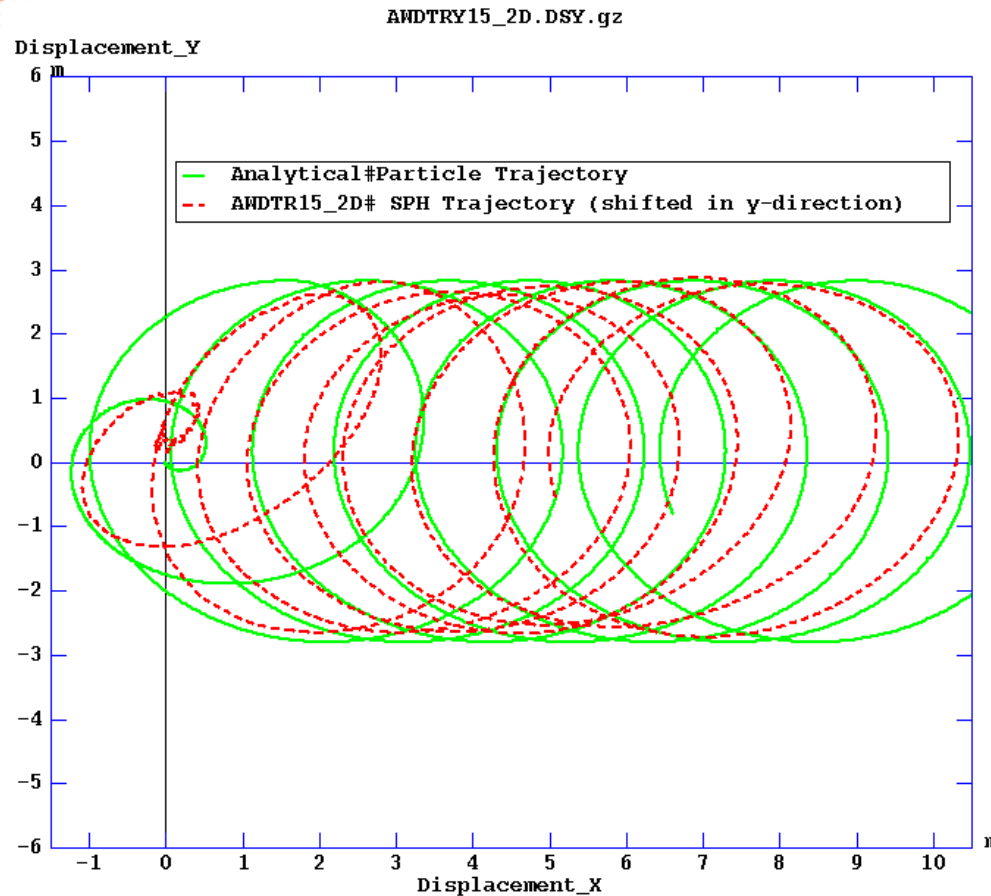
- Applicable to a full size ship, by implementing second order Airy displacements on the boundaries, we can generate a wave of 8 metres waveheight and 294m wavelength.





History of the vertical velocity of a selected particle compared to the analytical solution.

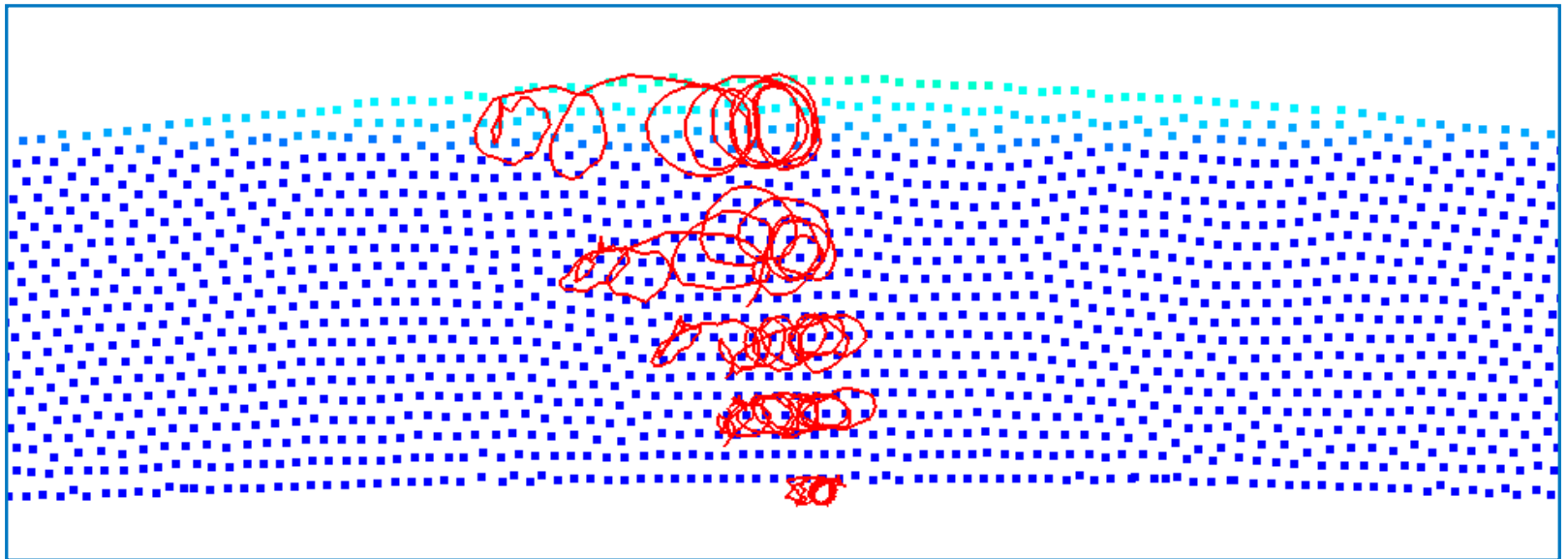




Trajectory of a selected particle compared to the analytical results. Since the particles tend to sink due to gravity there will not be a perfect match

## Deep Water Waves

Orbits of discrete particles within a wave illustrate that the particles at the junction of the SPH and the novel sea-floor interface have a circular motion, indicating that these deepest SPH particles are behaving as though they were in a deeper body of water



## Combination of waves with boat slamming

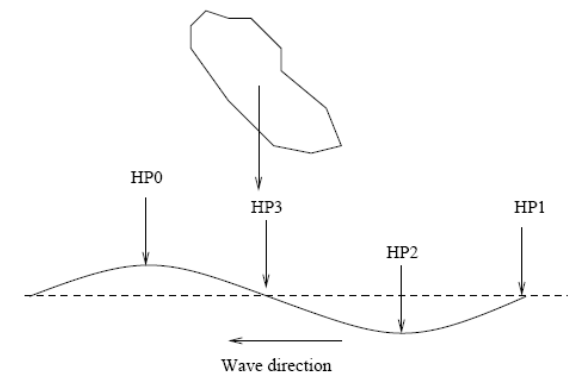
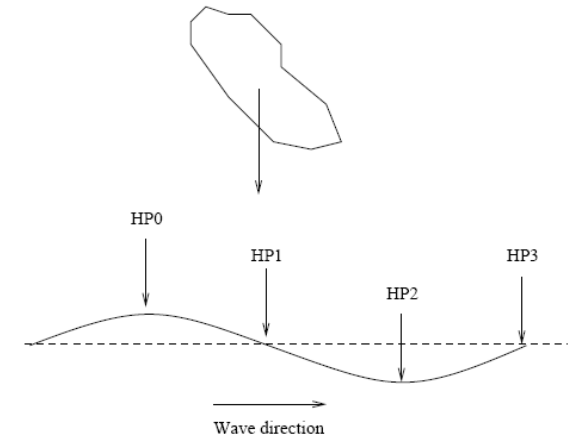
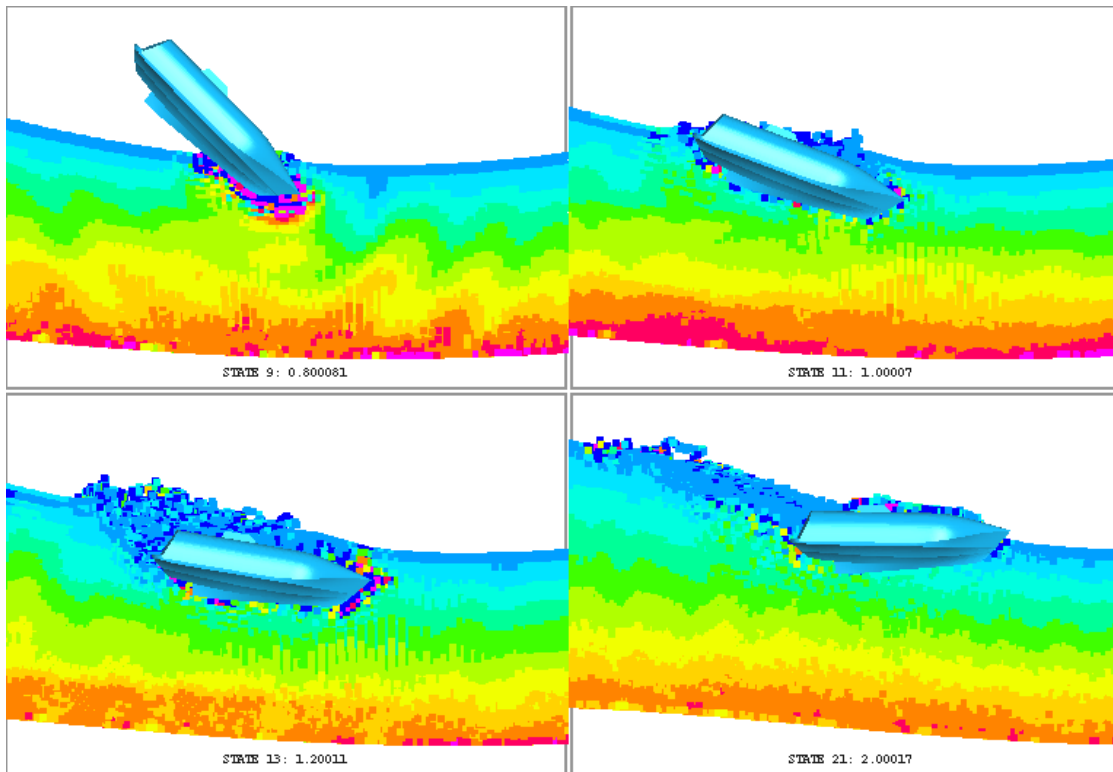
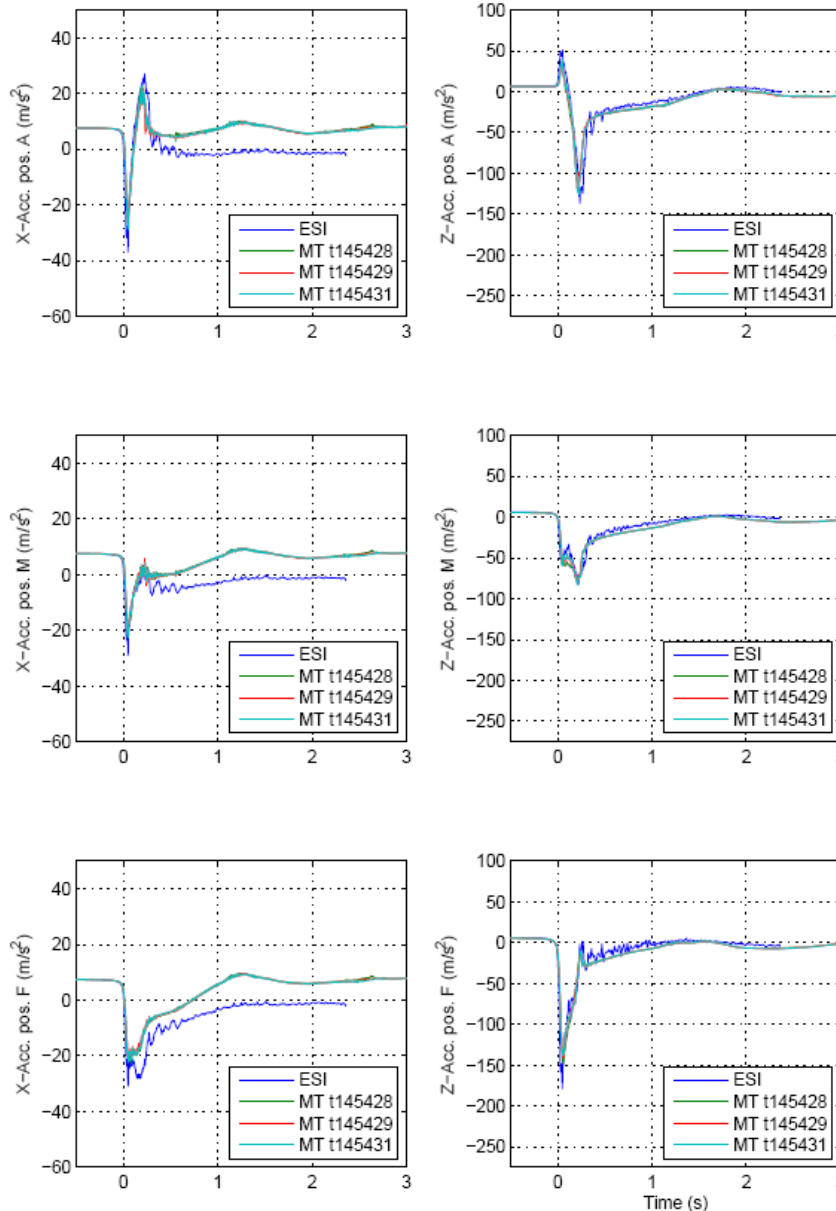


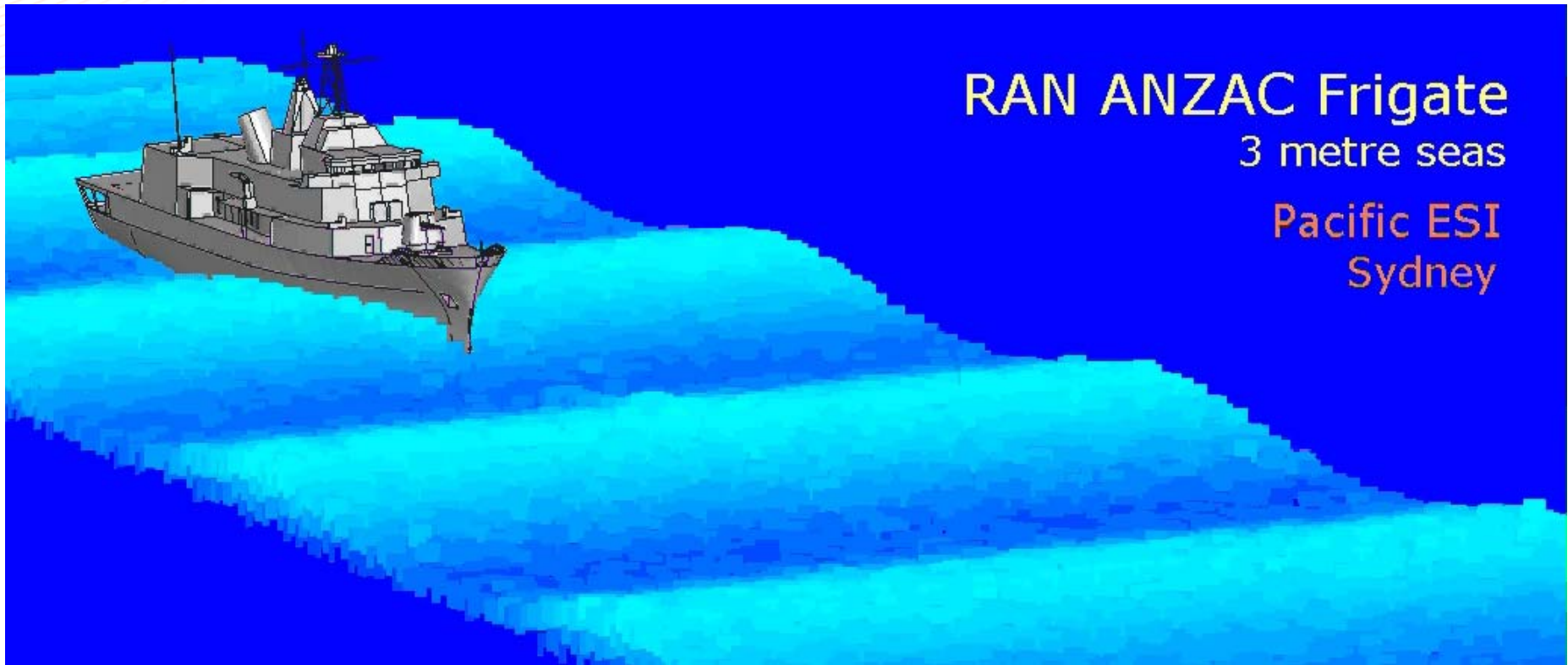
Figure 1.1: Hip point definition.

Drop height : 30m , Initial pitch : 50deg. Hit point : HP3 Wave dir. : Head



- The (x- and z-) accelerations from the PAM-CRASH simulations at 3 different locations at the hull of the LB have been compared to the results from 3 scale tests.

## Monohull in Head Seas



*A generic monohull is accelerated forward by a velocity boundary condition.*

*Cartwright, 2005.*

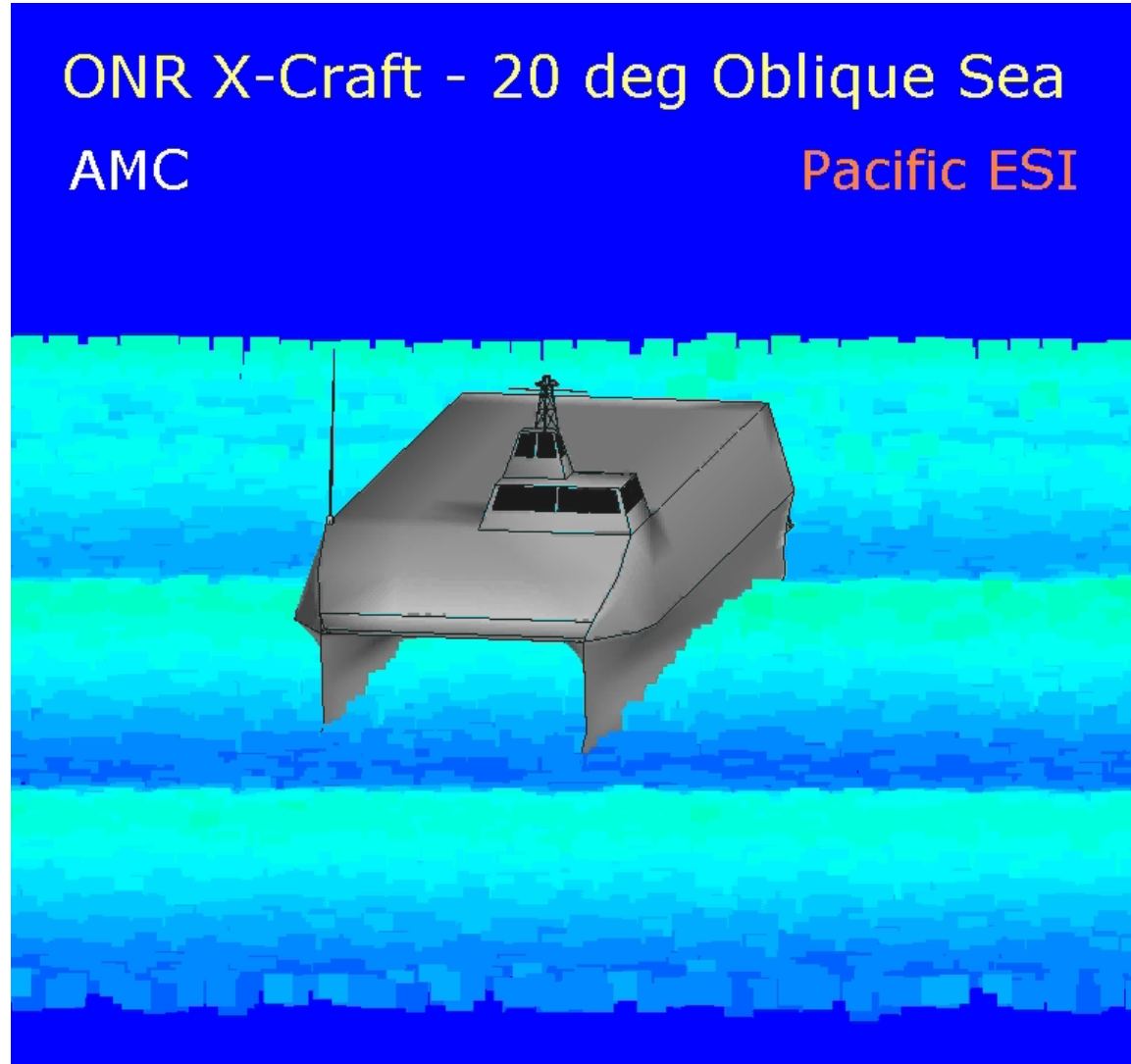


# Multihull in oblique waves

*A generic catamaran is propelled forwards at an angle to the waves.*

*Response of the vessel demonstrates pitch, yaw, heave and roll.*

*Cartwright et al, HPYD, 2006.*



# Amphibious Transport Ship

*Waves in the well dock*



## Phase 4A/B (acquisition of Landing Helicopter Docking Ship)





# Purpose of Study

1. Need to minimise risk associated with well docks
2. Define operational constraints of well dock operations
3. Develop numerical tools for landing craft tender evaluation

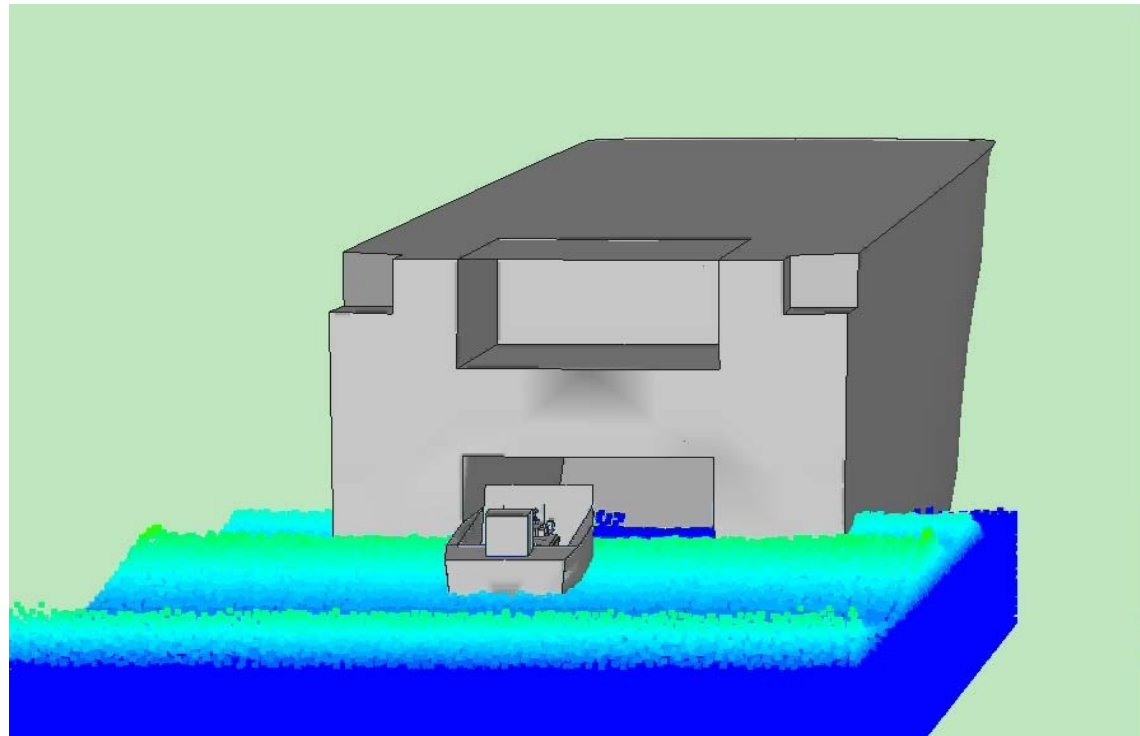
# Amphibious Transport Ship

## *Waves in the well dock*

An Amphibious Transport Ship (ATS), or Landing Helicopter Dock (LHD) ship, is a multi-purpose naval vessel to transport troops and equipment from sea to shore by a landing craft via a flooded well dock in the aft end of the ATS. The landing craft are subject to waves produced by the ATS motion and external waves.

Landing craft with 6 DOF.

Asymmetric thrust on entering well dock produces a collision with wall. Large peak forces result.

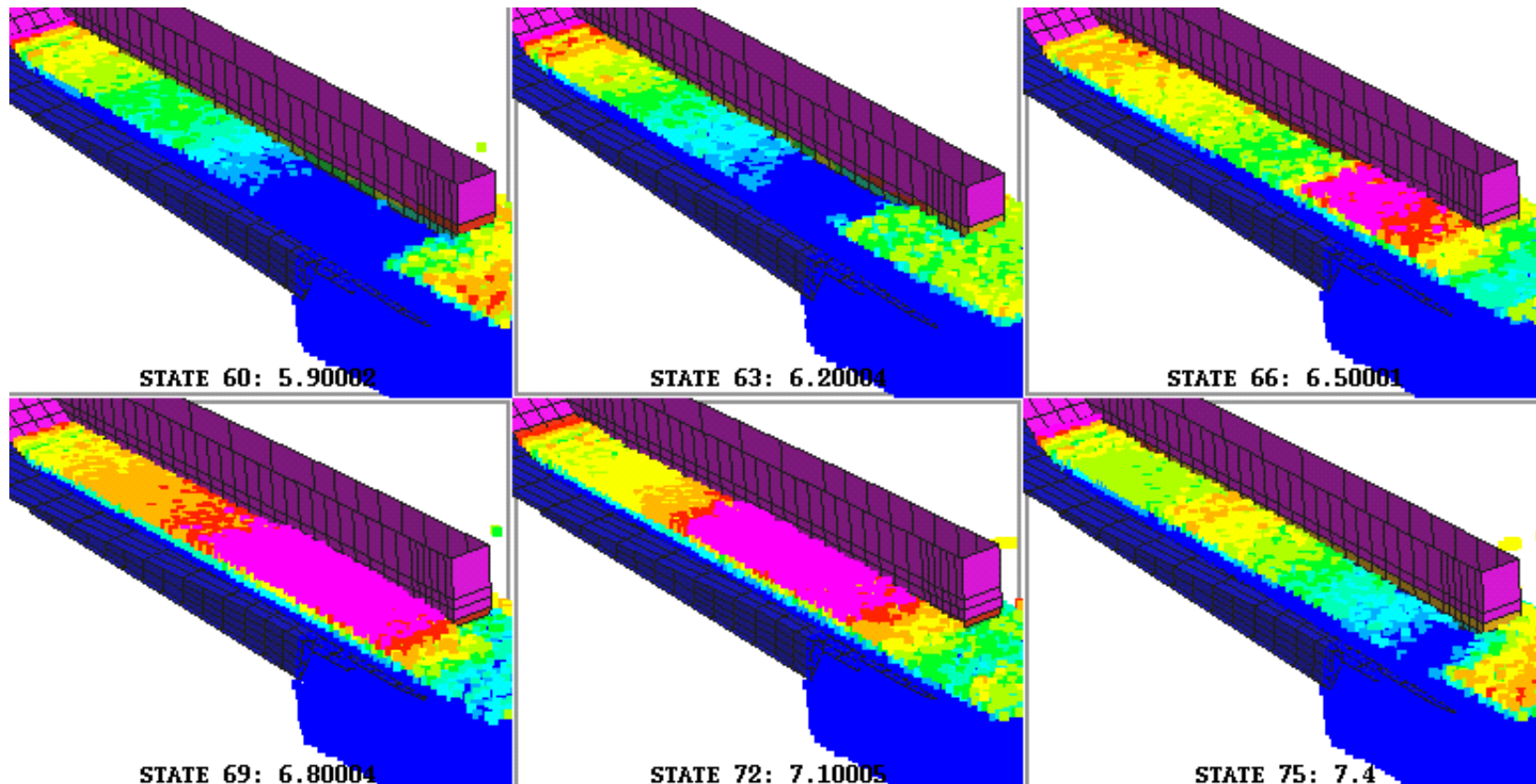




# Amphibious Transport Ship

## *Waves in the well dock*

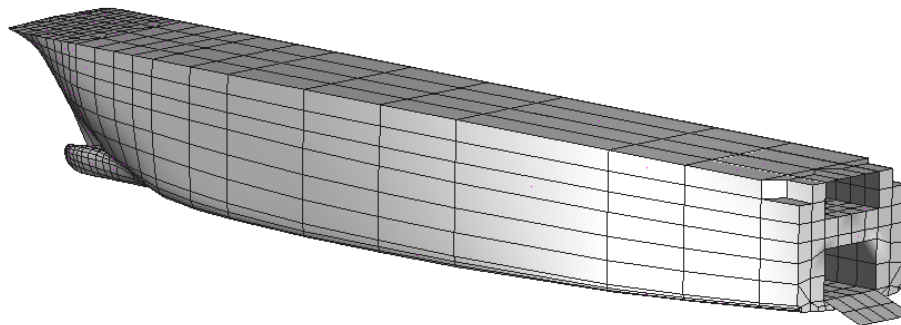
A perspective aerial view into the cut-away section of the well dock at the aft end of the ATS model. (Deck removed for clarity) Colour contour represent wave height (range -0.01 .. 0.03 m).



# Numerical Analysis Setup Overview

## LHD Model

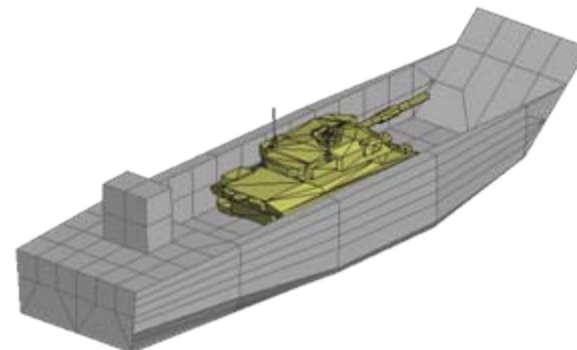
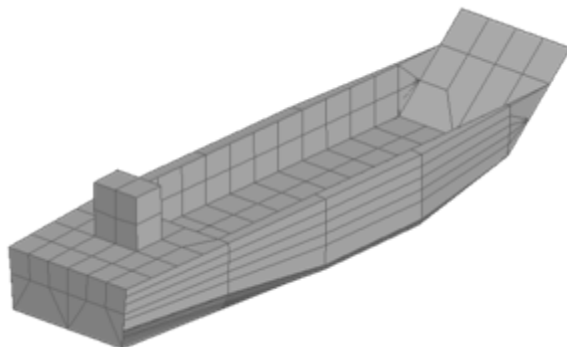
<b>Length overall (LOA) (m)</b>	210
<b>Beam (m)</b>	33
<b>Draft at COG (m) (with flooded well dock)</b>	7.6
<b>Trim angle when flooded</b>	Trim by stern 1.8 m
<b>Well Dock Dimensions</b>	
<b>Length (m)</b>	70.0
<b>Width (m)</b>	14.8
<b>Mass (tonnes)</b>	26000



# Numerical Analysis Setup Overview

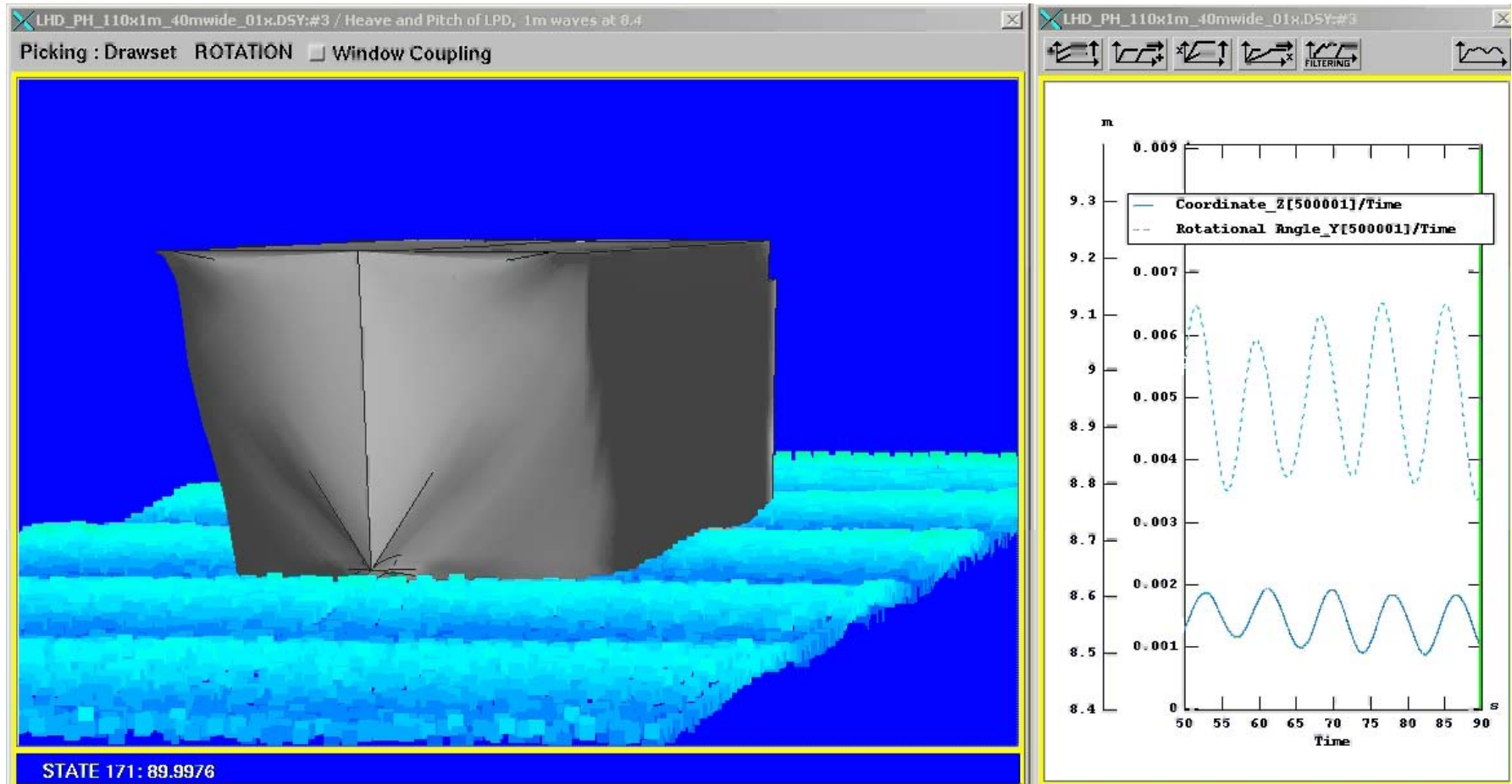
## Landing Craft Models

Length overall (LOA) (m)	24.5	
Beam (m)	6.4	
Mass (tonnes)	Model 1 (Light) 42.8	Model 2 (Heavy) 90.4
Longitudinal COG from FP (m)	11.1	9.6
KG at midships (m)	1.366	1.852
Draft at Midships (m)	1.14	1.68



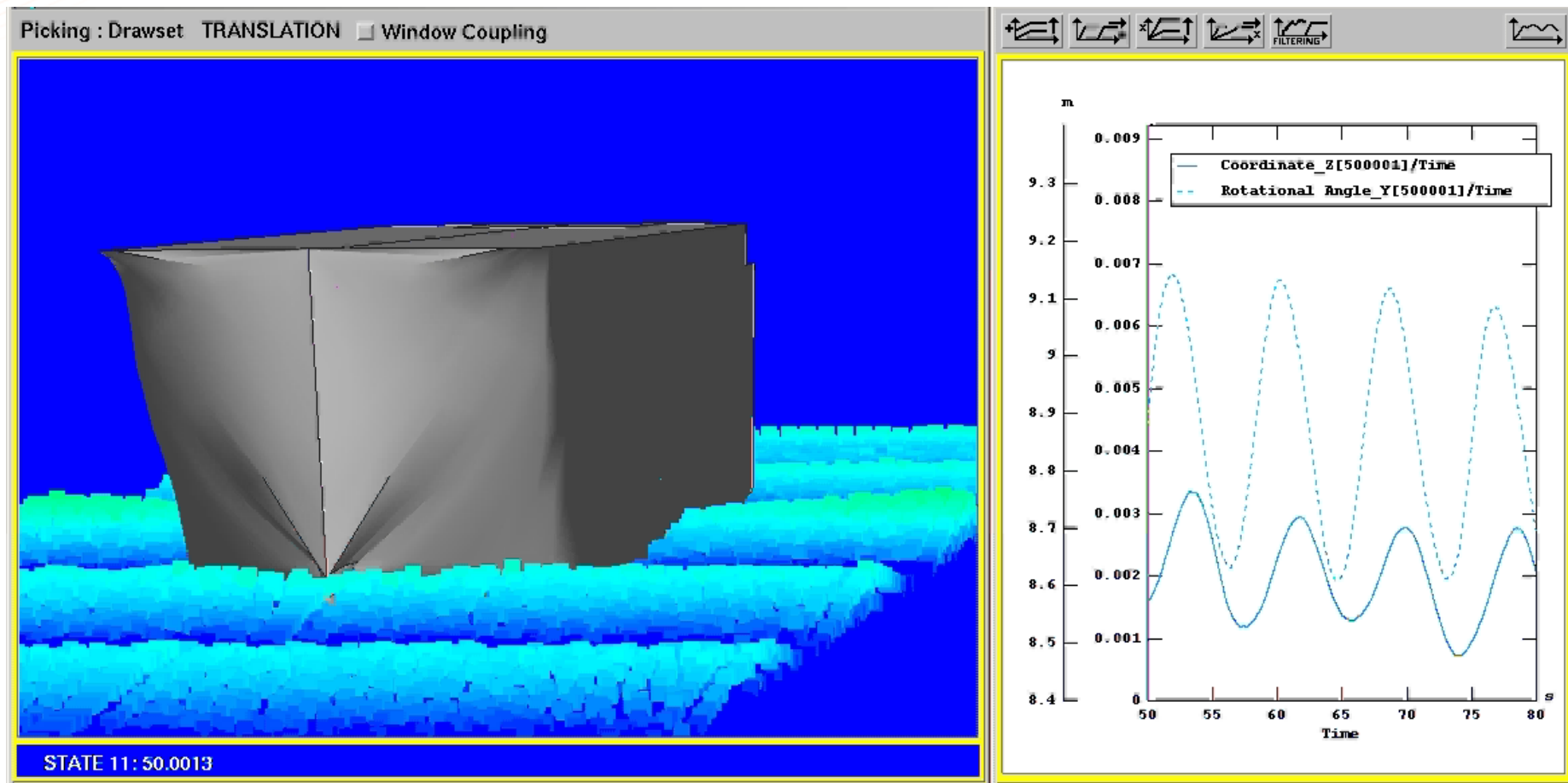
# Results and Observations

## LHD Motions – Pitch and Heave in 1m sea



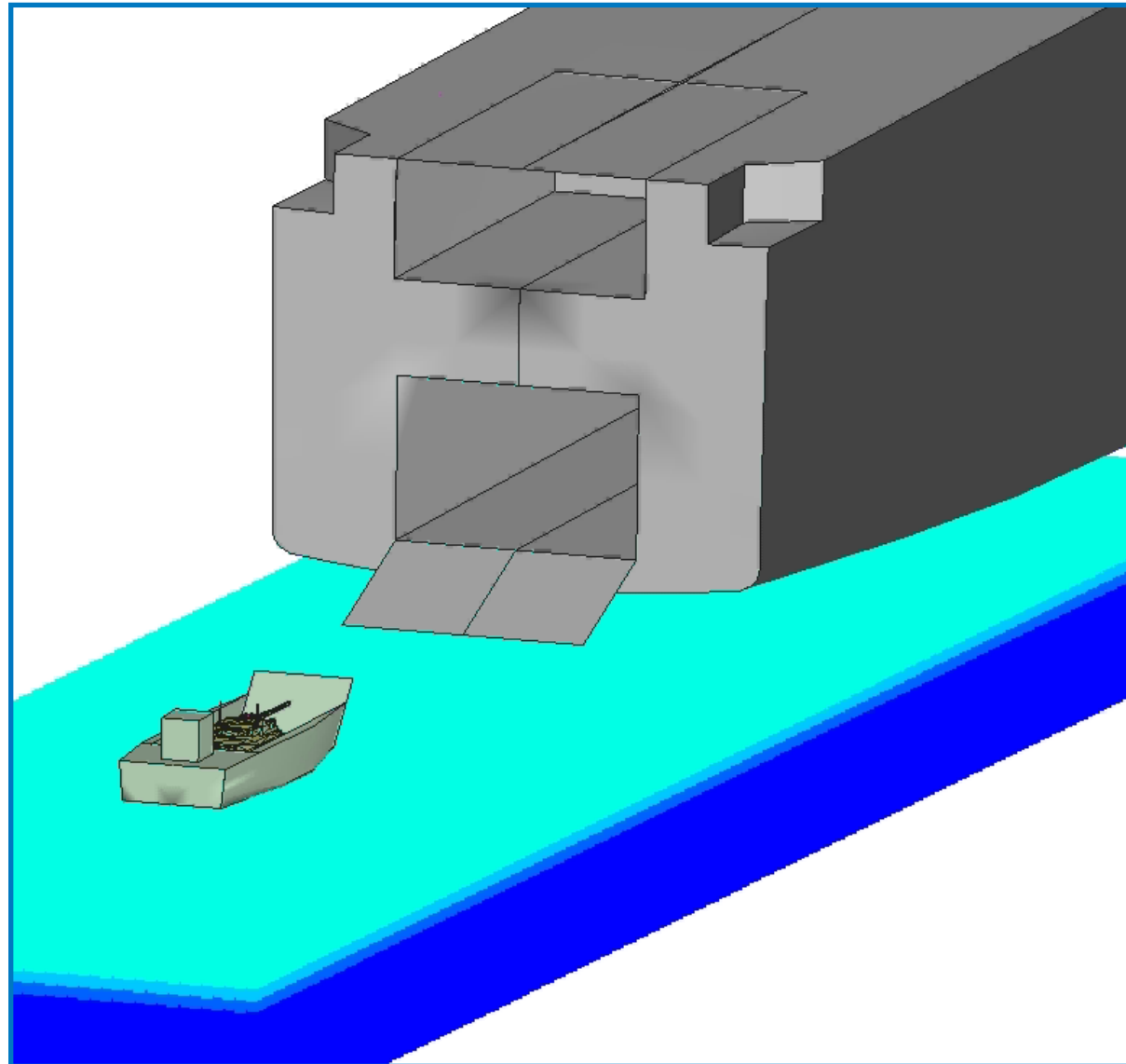
# Results and Observations

## LHD Motions – Pitch and Heave in 2m sea



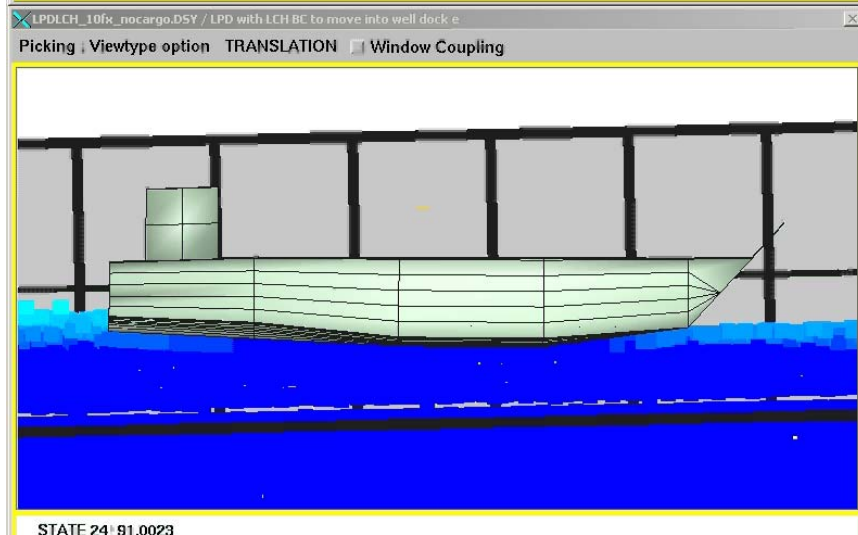
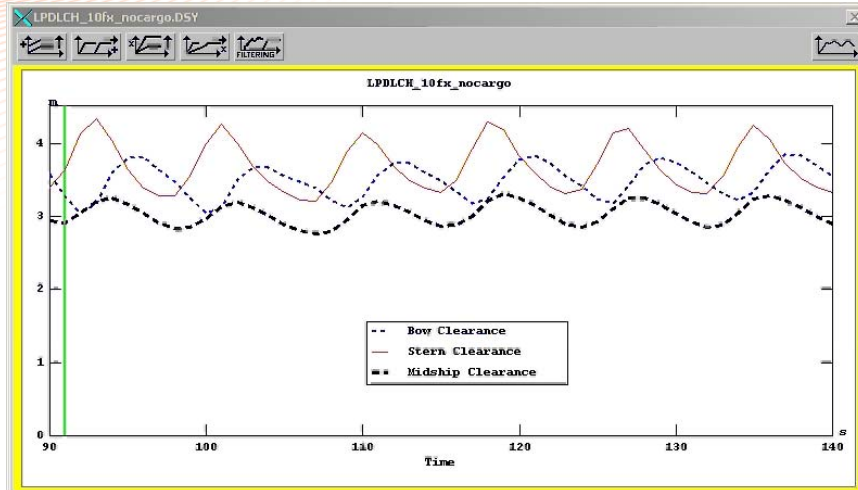


# Landing Craft Motions

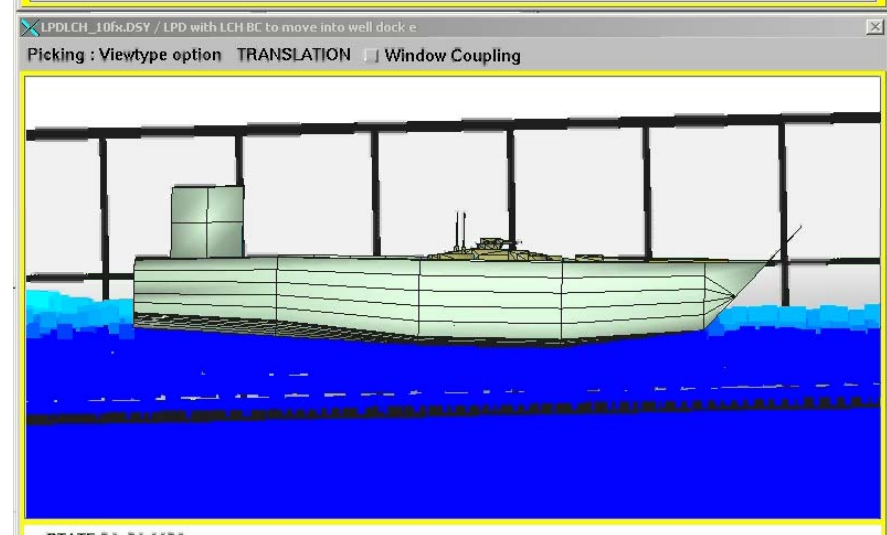
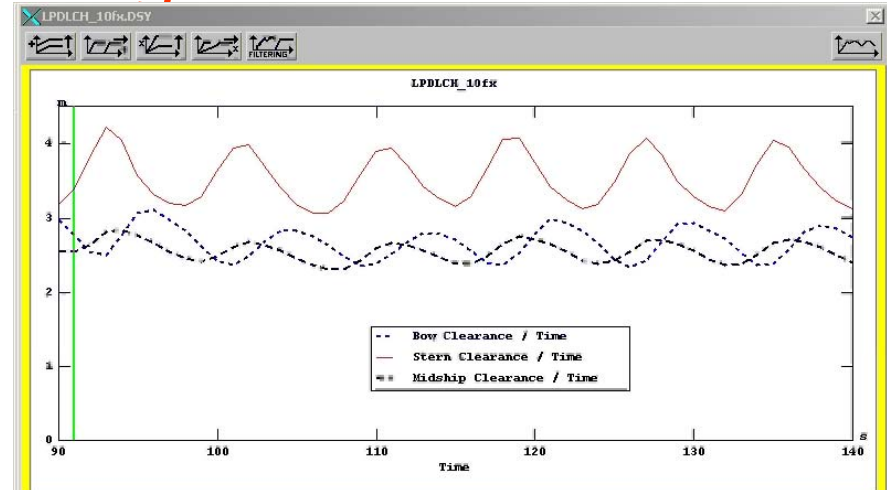


# Results and Observations

## Clearance Under the Landing Craft at Mid-Dock



**No Payload**



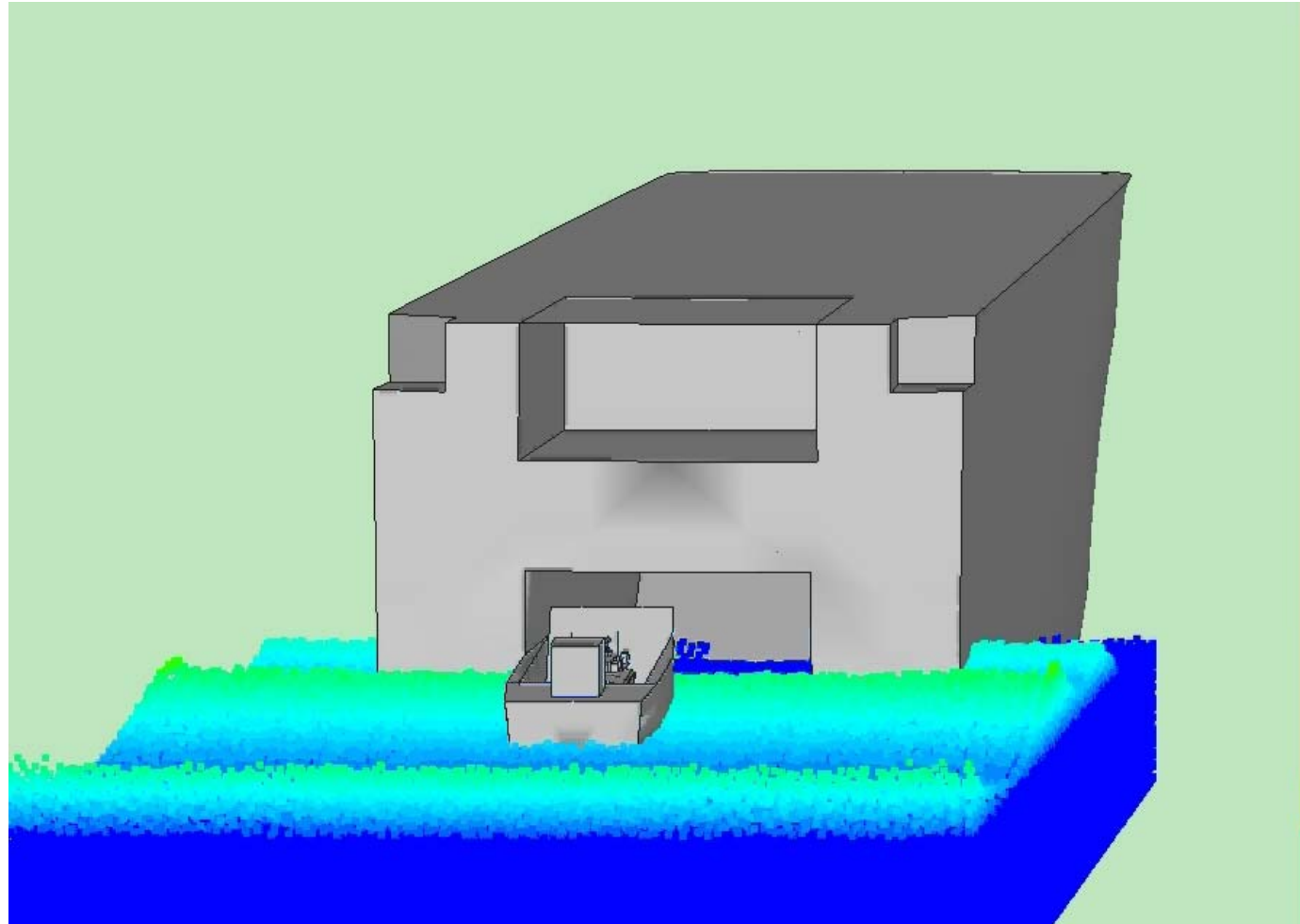
**Payload**

# Results and Observations

## Rough Landing Scenario

Landing craft  
with 6 DOF.

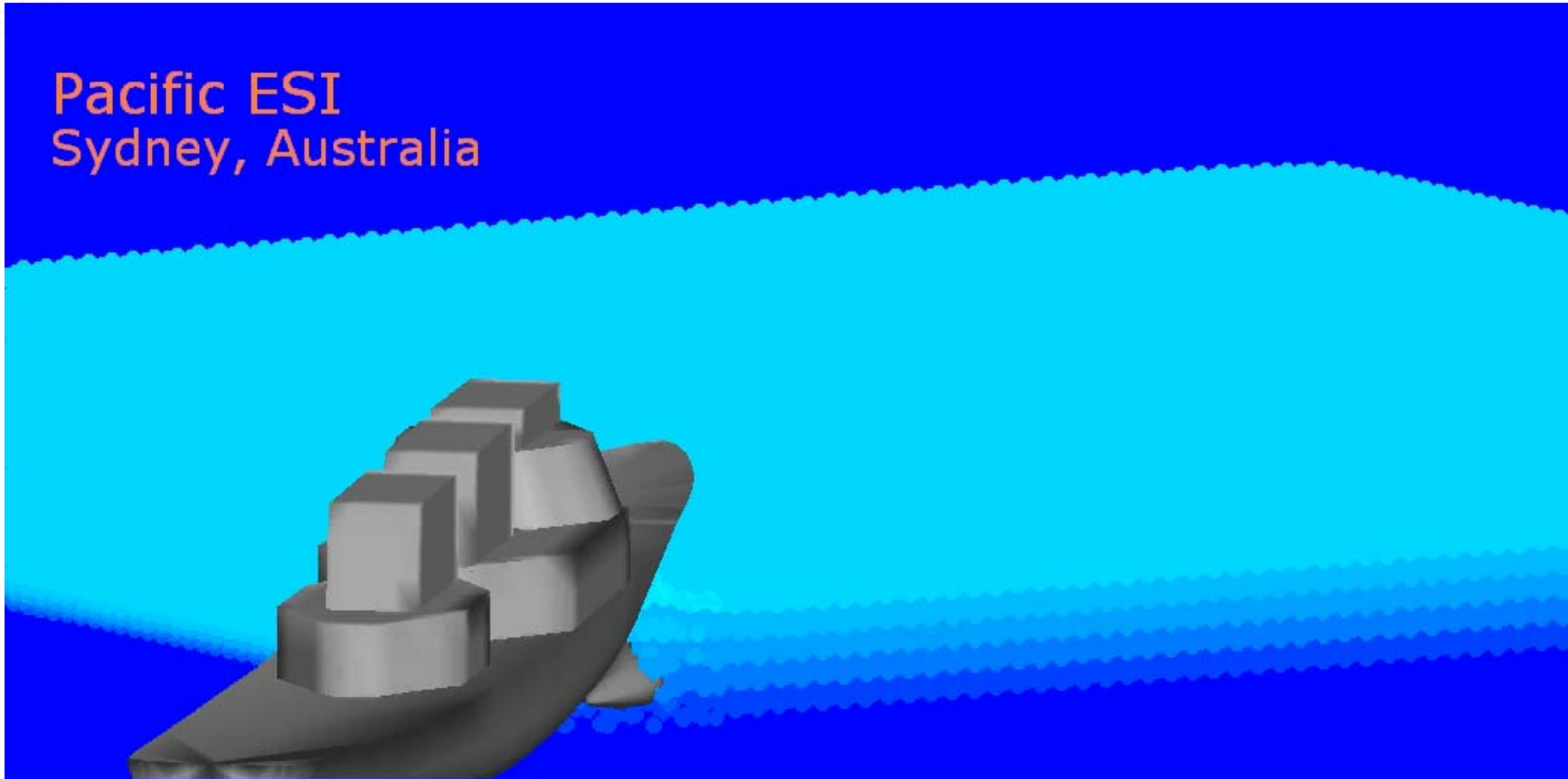
Asymmetric  
thrust on  
entering well  
dock produces  
a collision with  
wall. Large  
peak forces  
result.



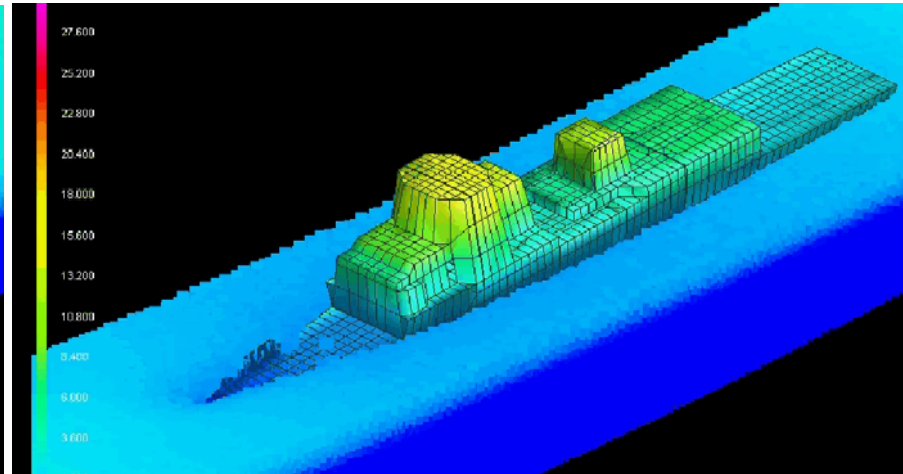
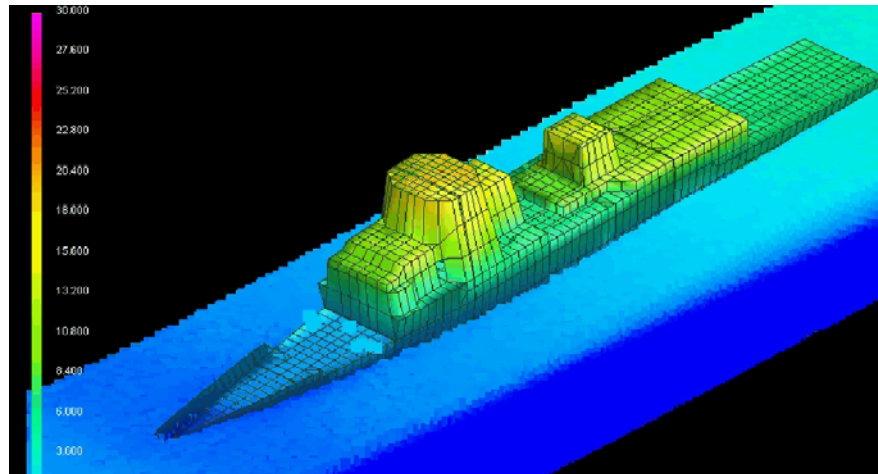
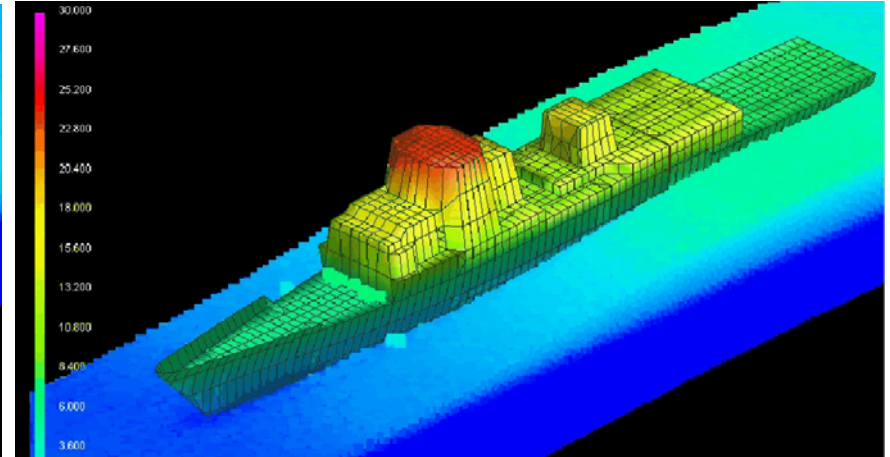
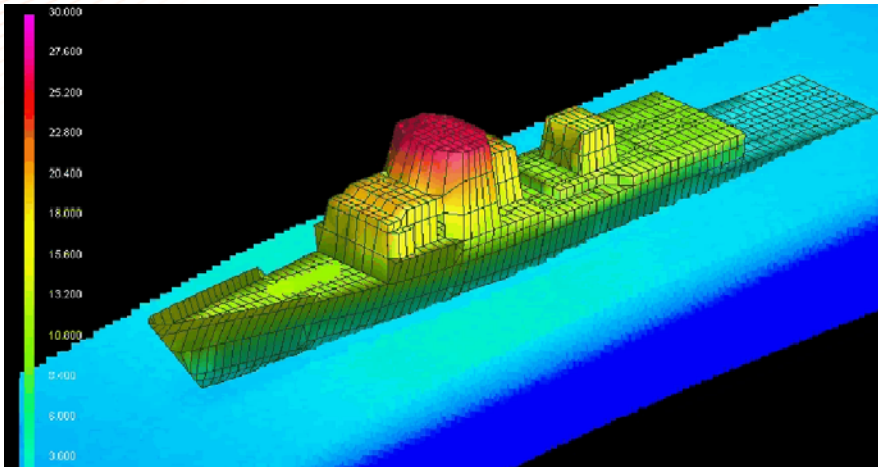


# Fast frigate in heavy seas

Pacific ESI  
Sydney, Australia



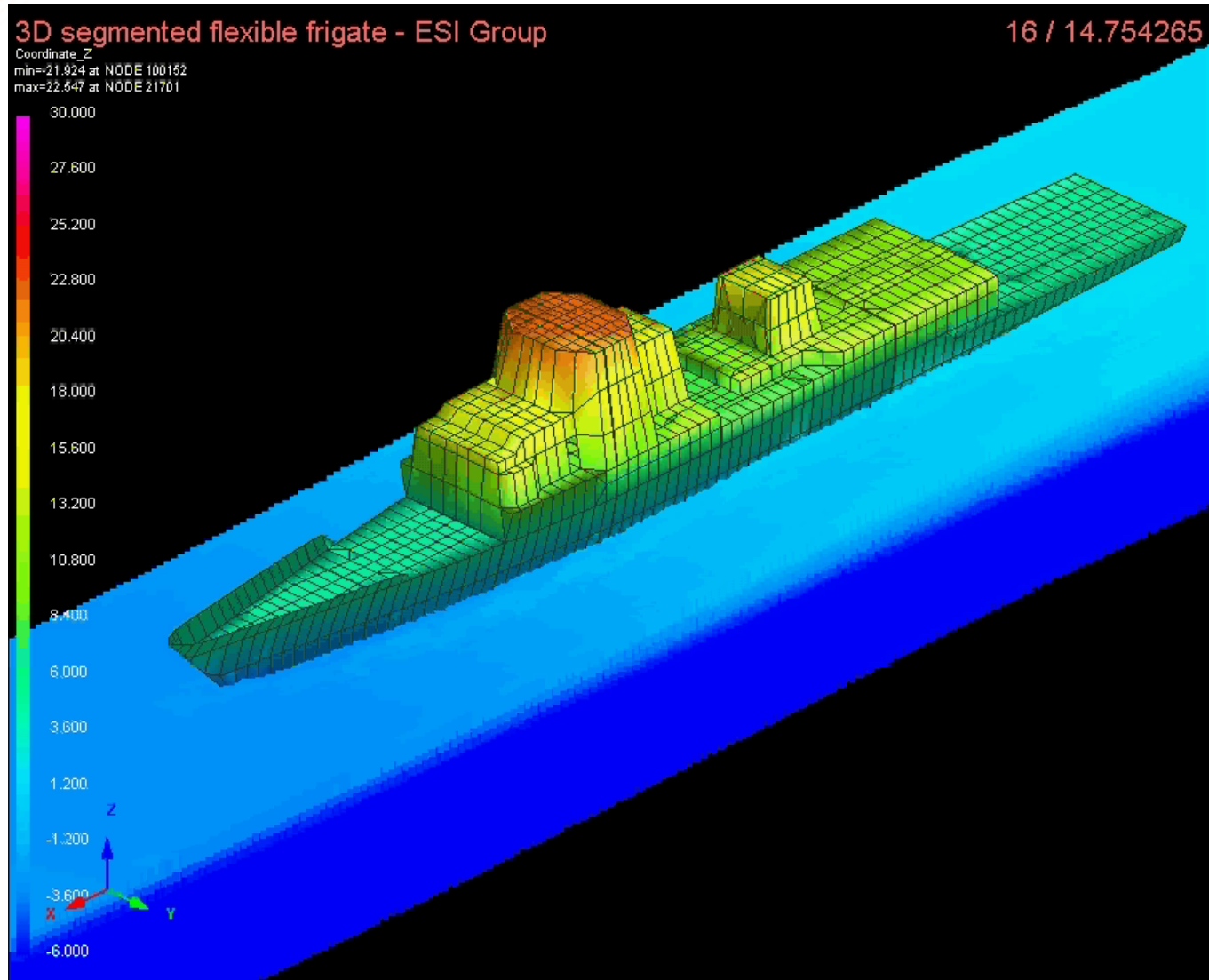
Regular head waves of 8 meter height and a wave length of 294 meter

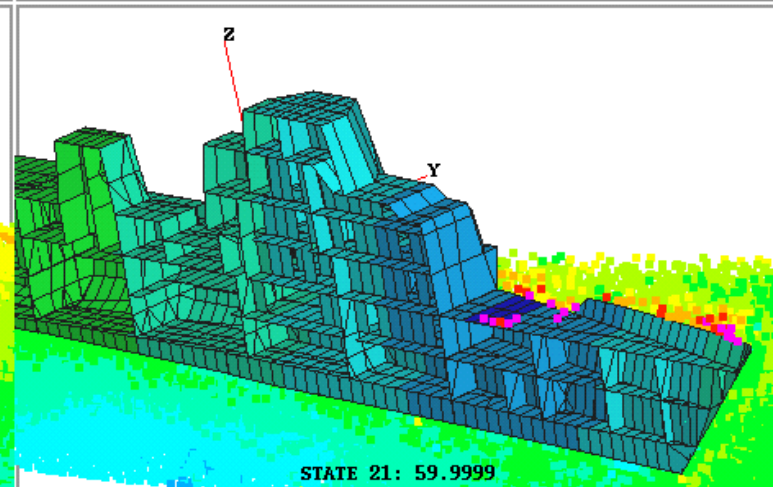
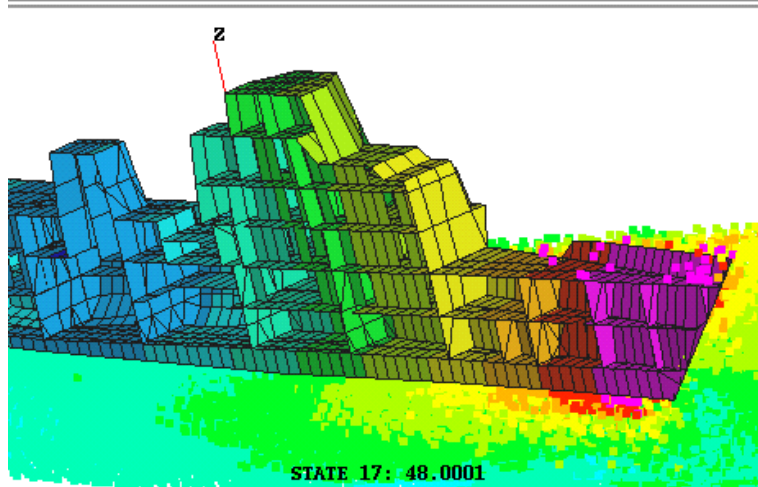
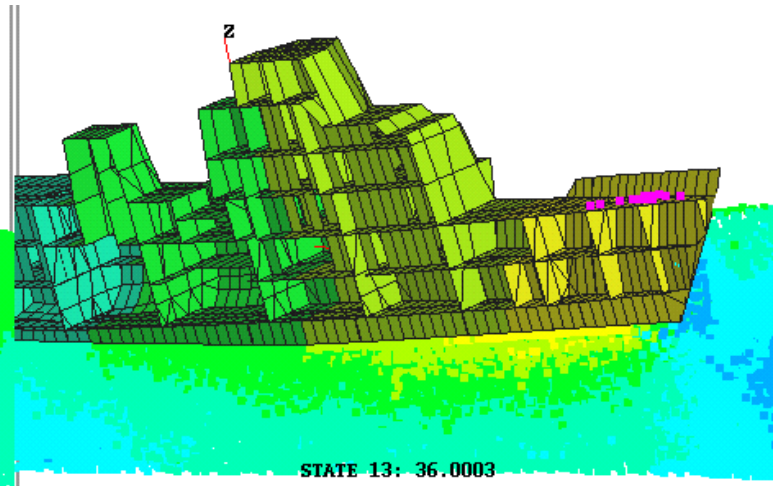
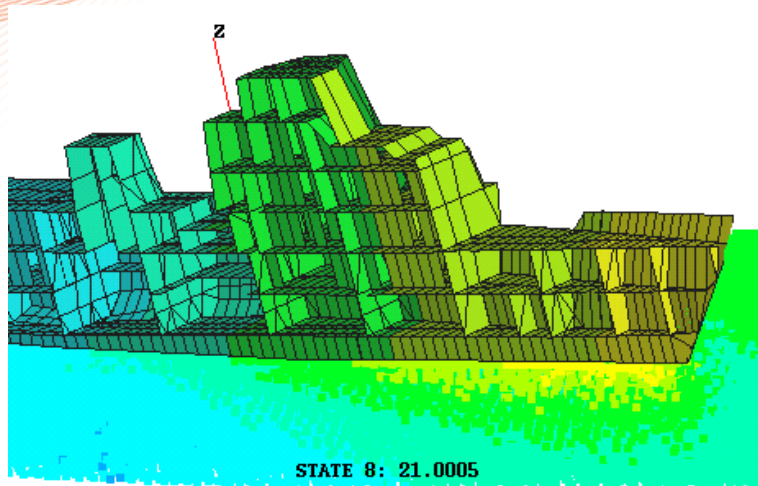
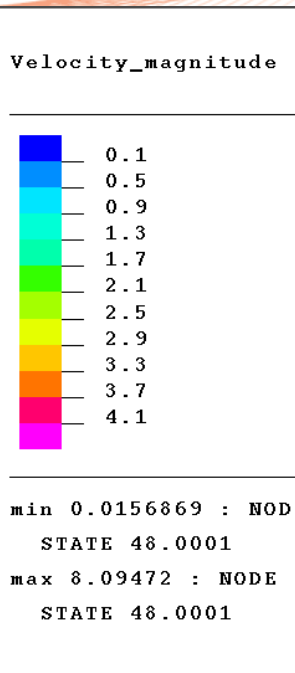




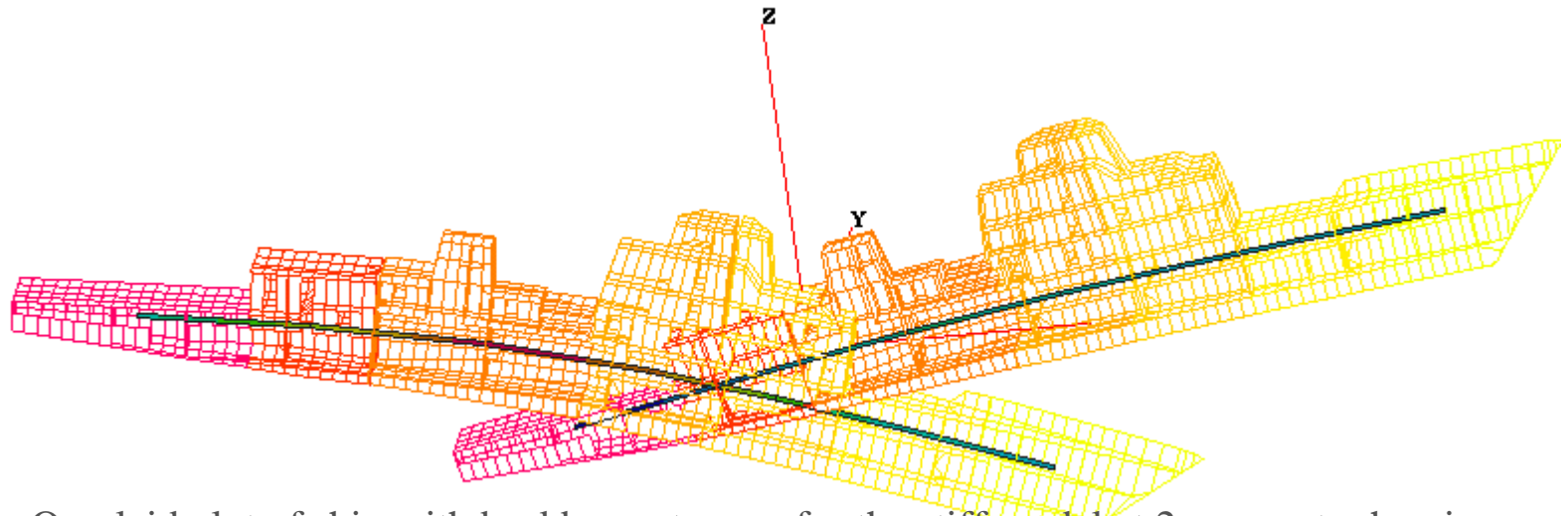
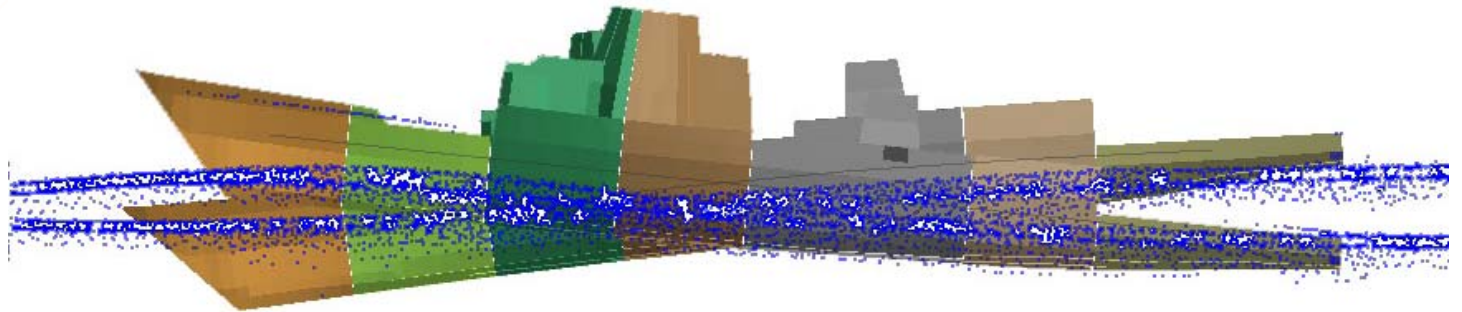
# Generic Frigate Model

Vertical/bending moment/velocity for flexible model



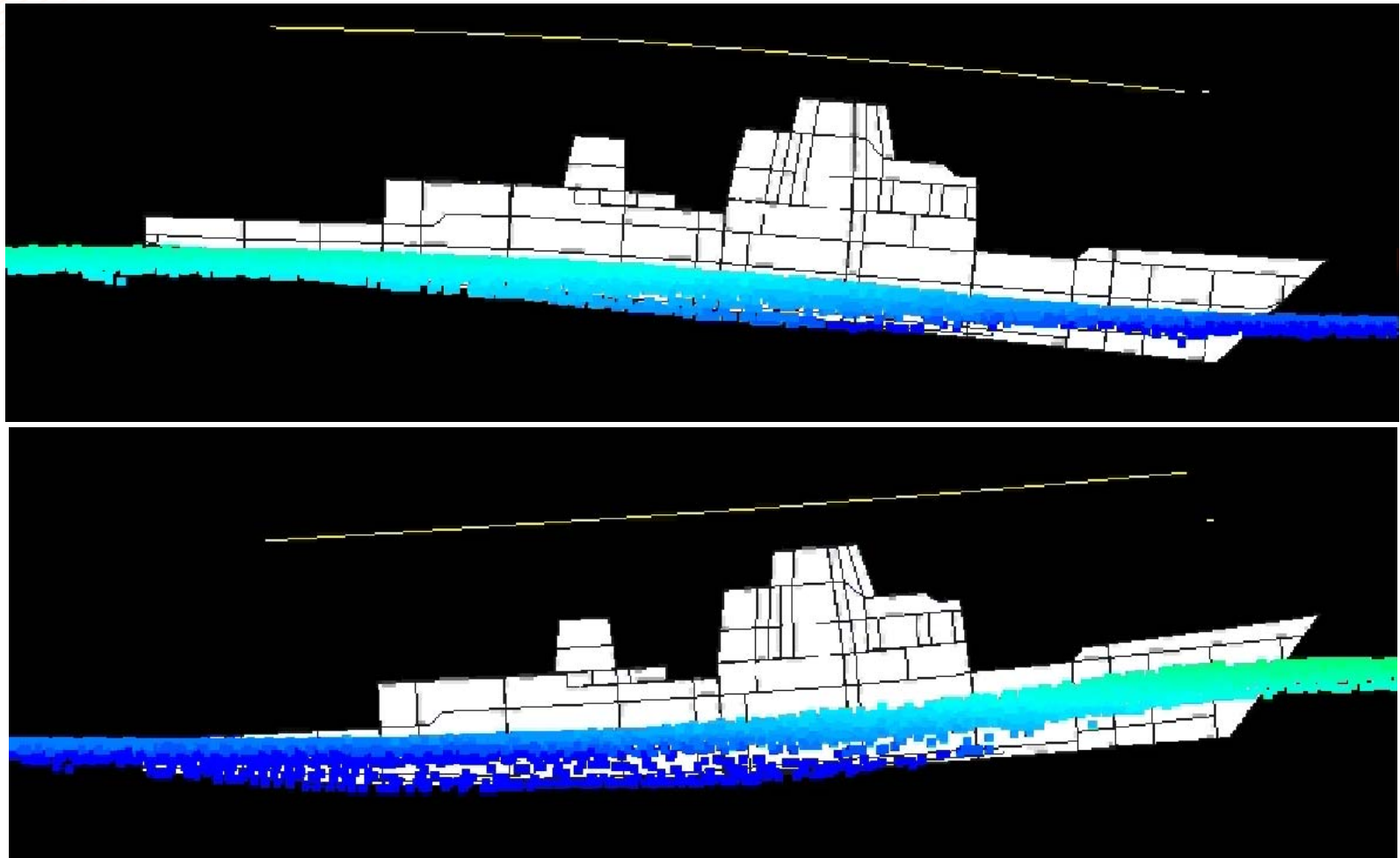


Display of the velocity magnitude for the flexible model in waves.



Overlaid plot of ship with backbone stresses for the stiff model at 2 moments showing the motion and bending at 21 and 60 seconds (displacements scaled by a factor of 4).

Side view of the backbone deformations



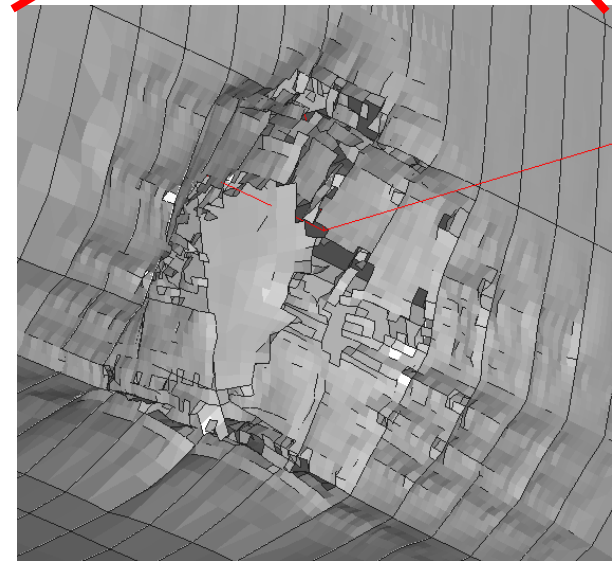
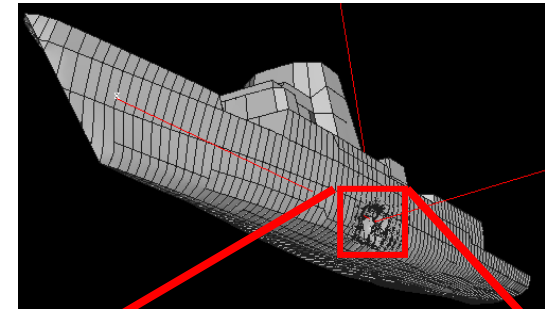


# Vessel subject to UNDEX

Smoothed Particle  
Hydrodynamics

**PAM-SHOCK  
and  
PAM-CRASH**

**For Naval Applications of:  
Underwater Explosion,  
Fluid-Structure Interaction,  
and  
Damage and Flooding Prediction**





# “Ductile” metallic rupture

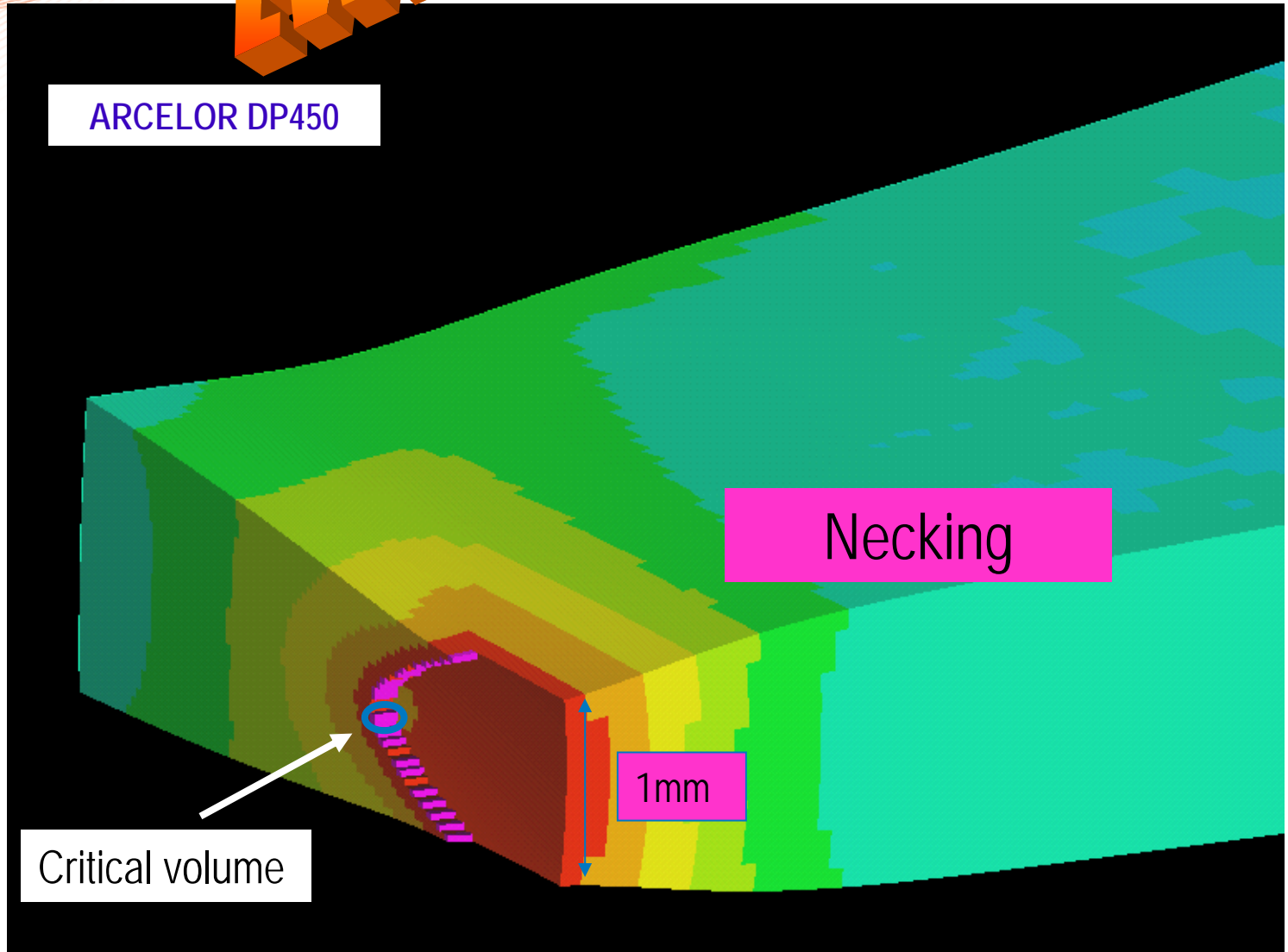
EWK

ARCELOR DP450

Necking

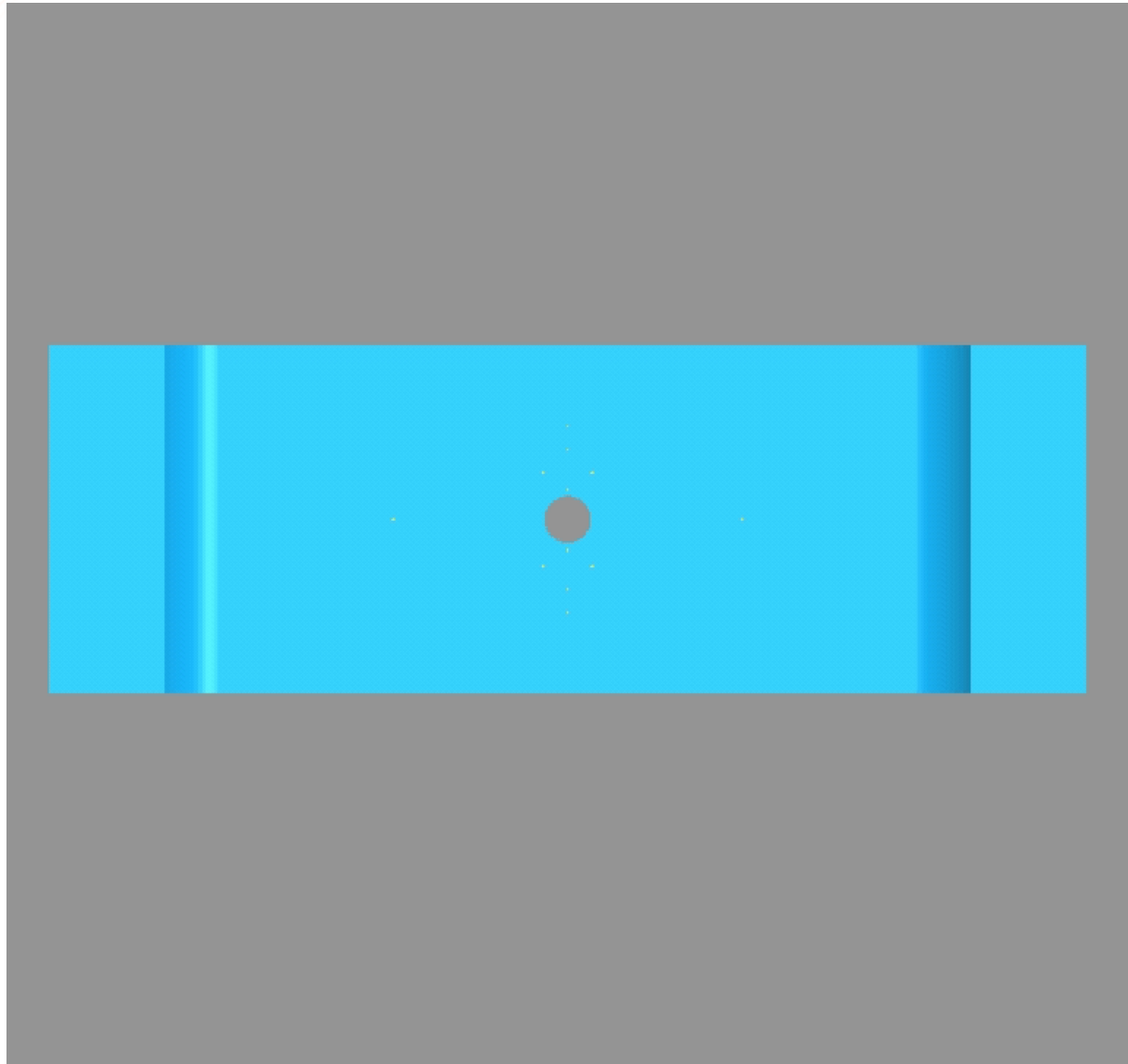
1mm

Critical volume

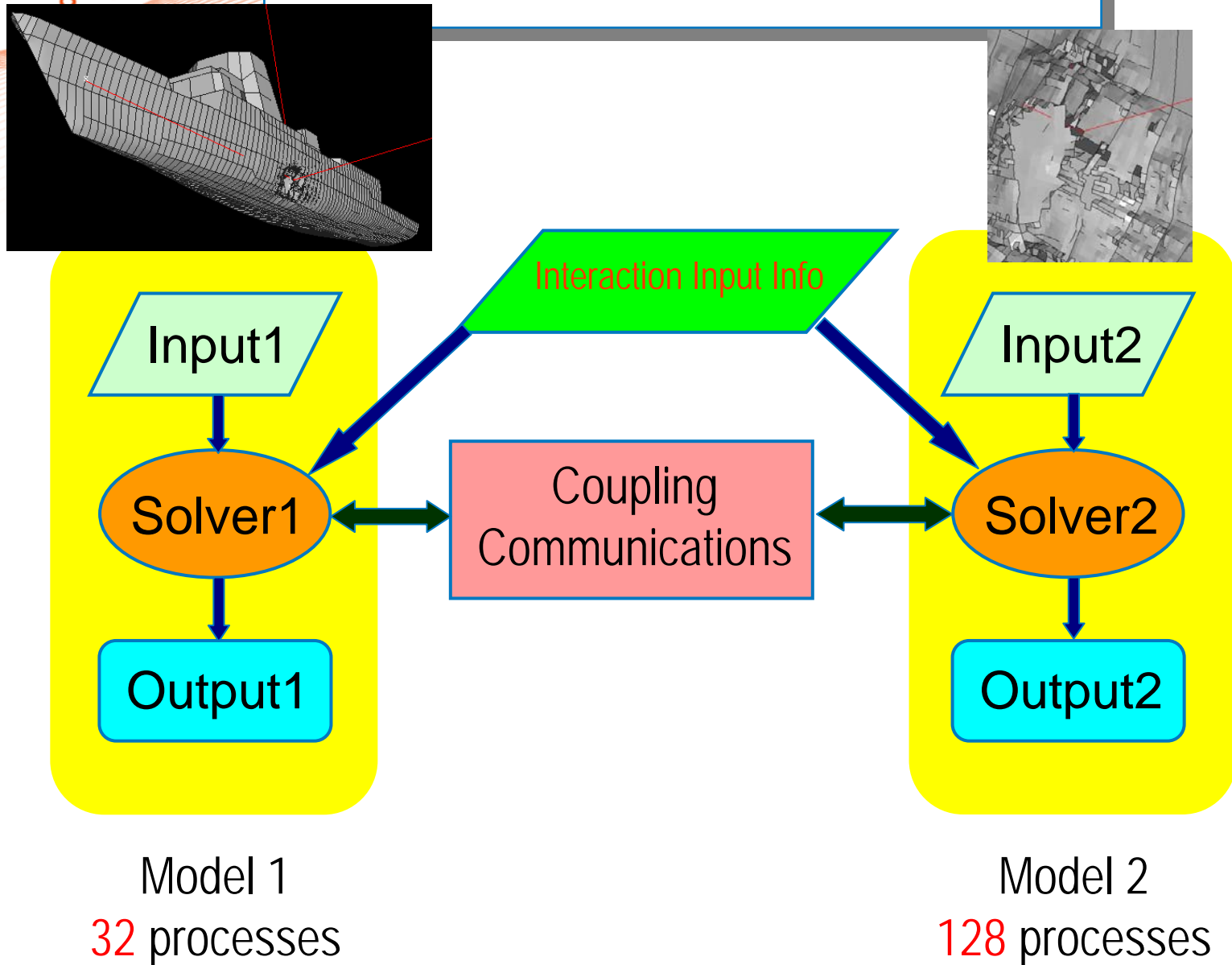


# Effect of stress concentration

**EWK**



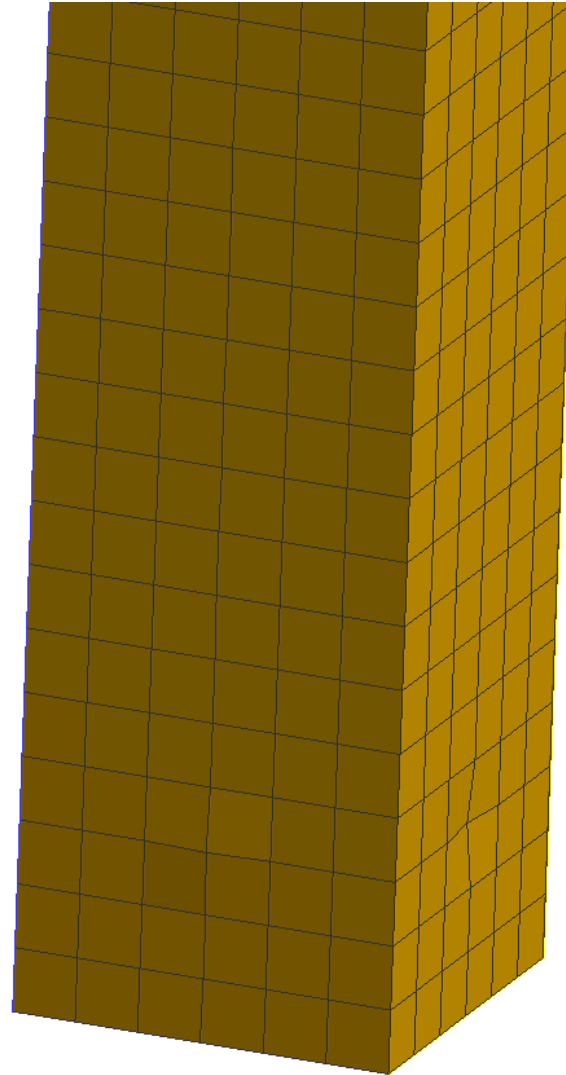
## Multi-Model Coupling for Multi-Scale calculations



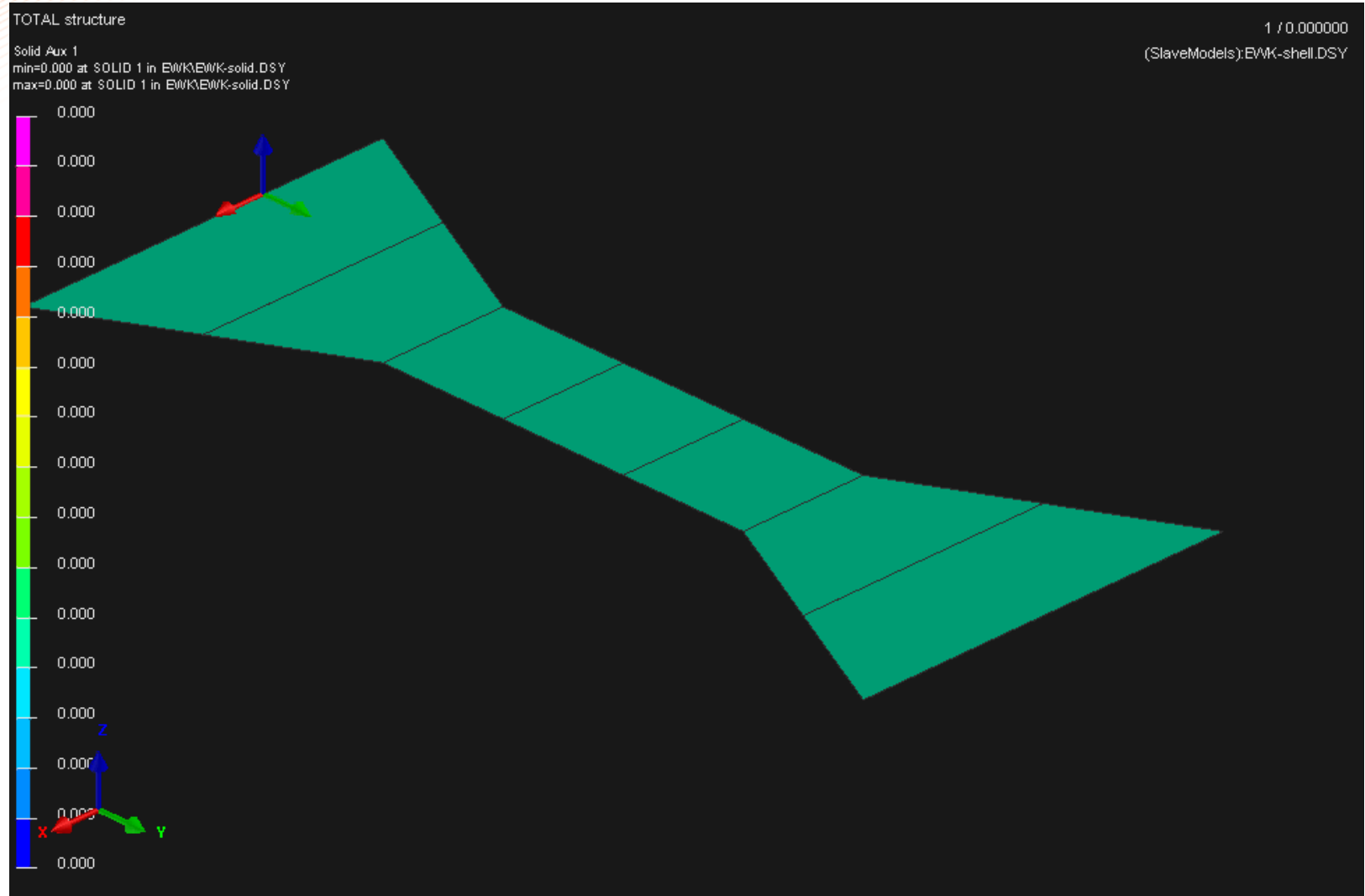
# Automatic shell to solid transition

TOTAL structure

1 / 0.000000  
(SlaveModels)box2002.DSV



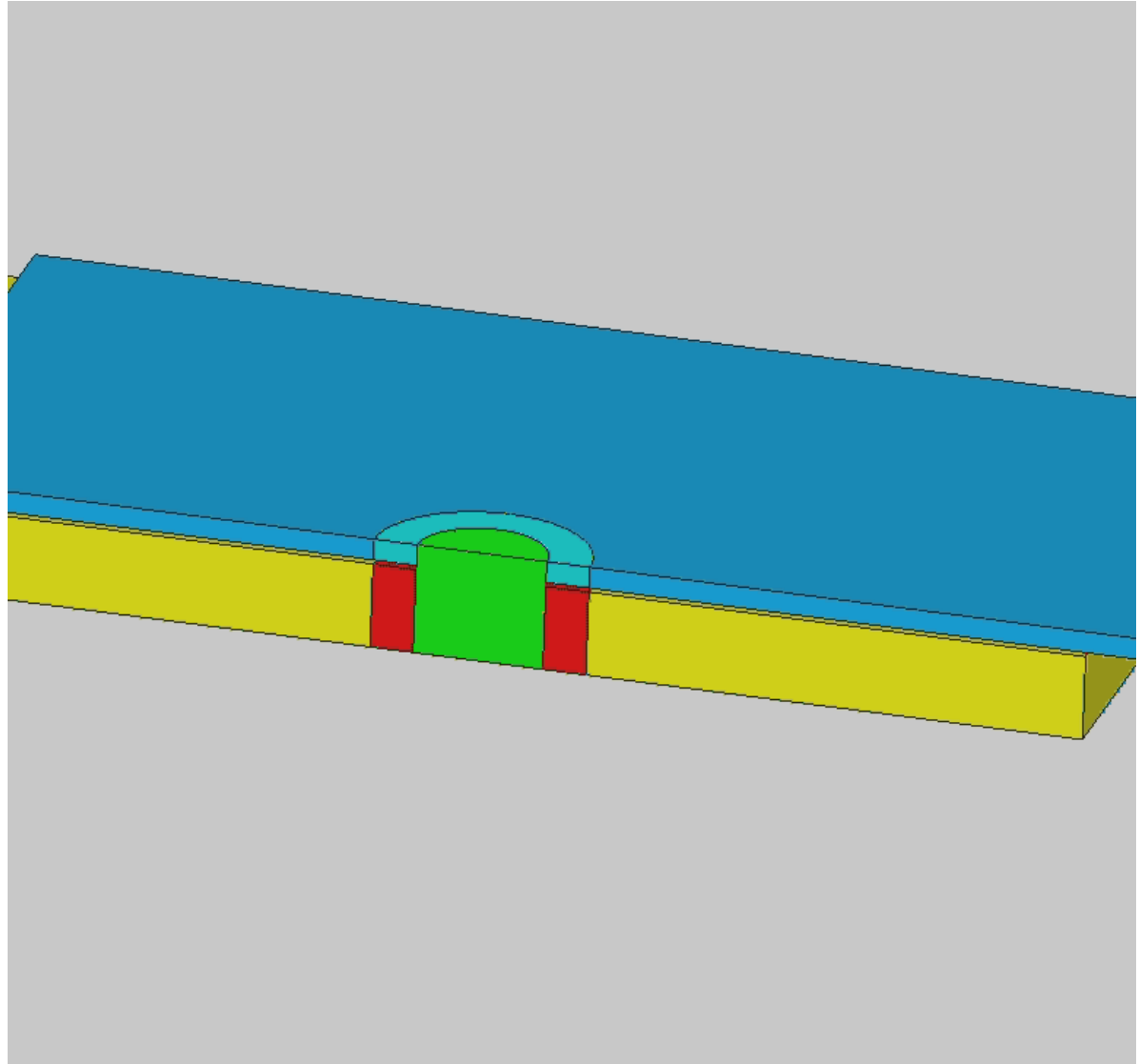
## Automatic shell to solid transition

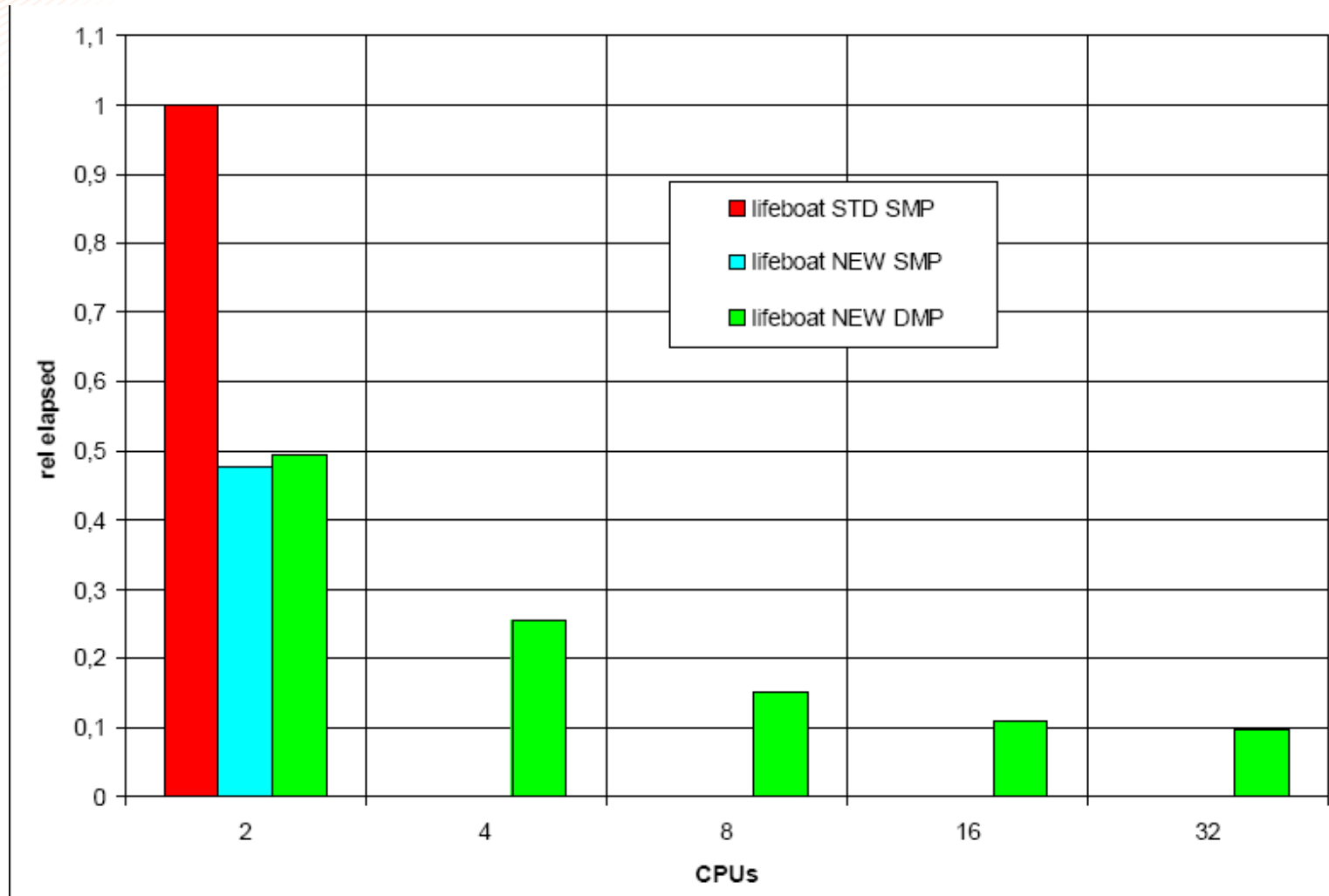




# EWK model for efficiently predicting connectors

And either calibrate macro elements for efficient handling of hybrid FE large models, or perform intrinsic and predictive calculations through the **Multi-Model Coupling** option



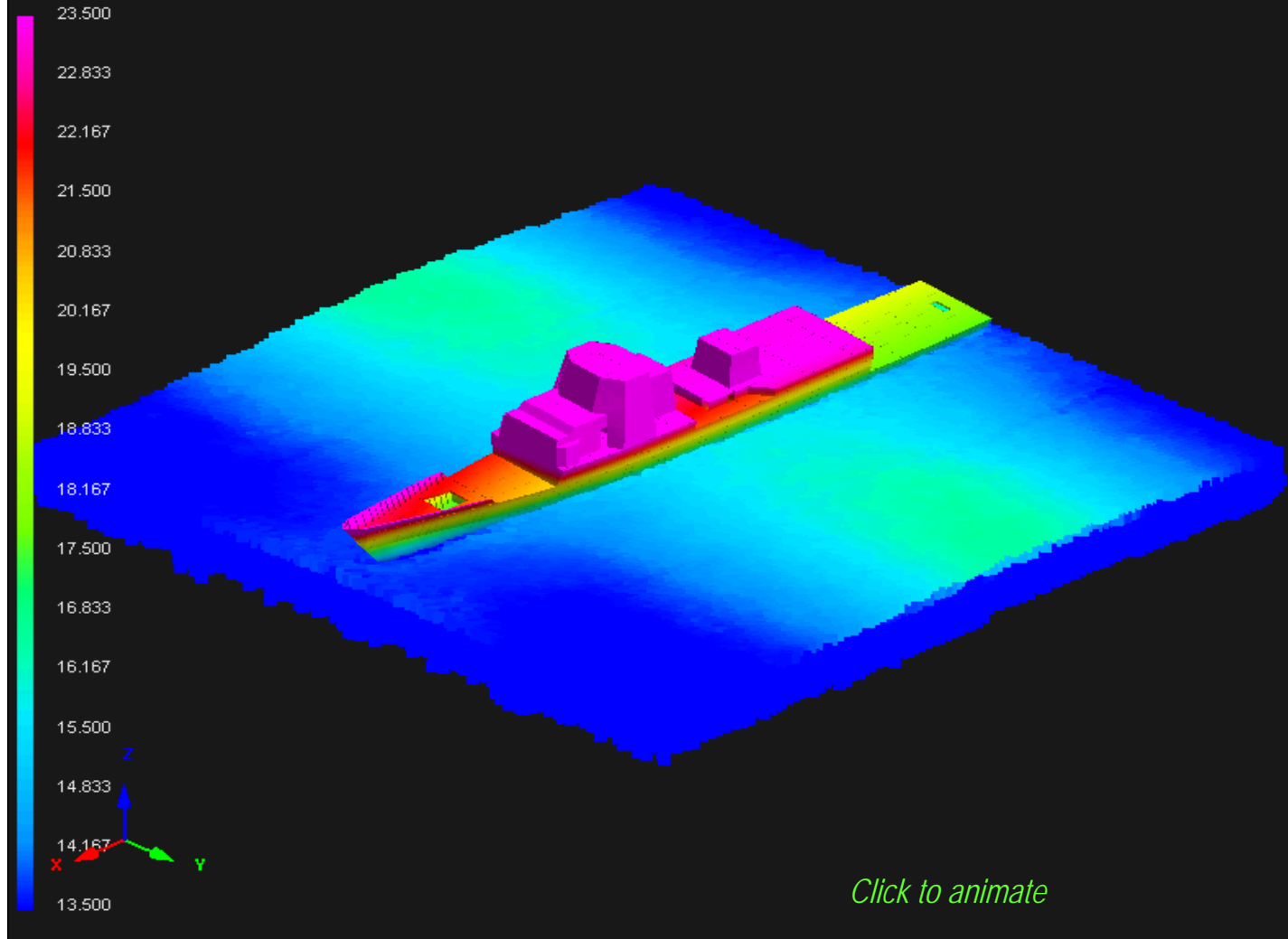


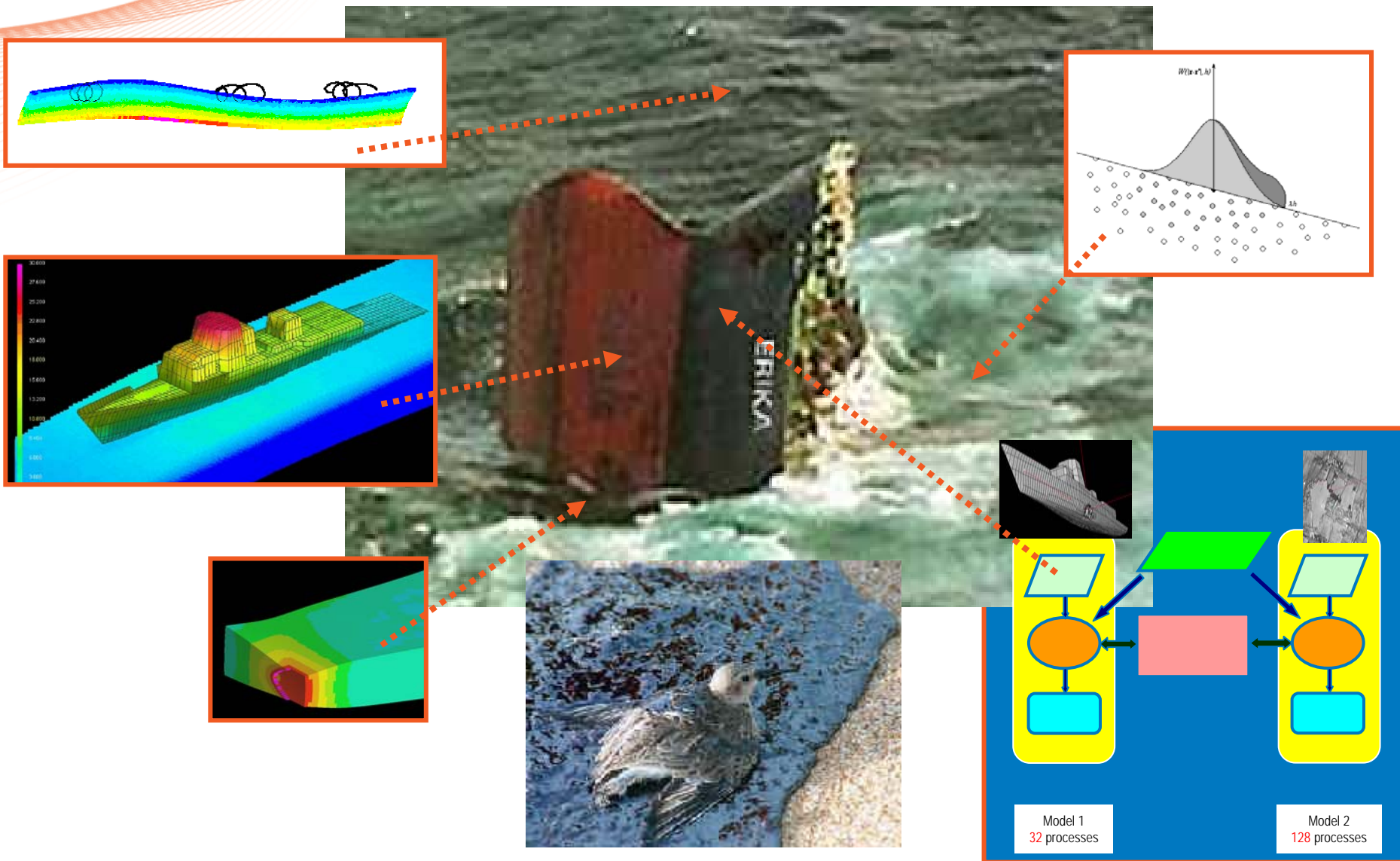
*Response of  
damaged  
vessel*

*Note the  
initial list to  
port  
indicating  
flooding*

Generic Frigate Stability Study - Hull Breached Due to UNDEX  
Coordinate\_Z  
min=-0.568 at NODE 2054965  
max=38.350 at NODE 4102

110 / 66.105621





Thank you !